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Coherent beam combining techniques : an introduction

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Coherent beam combining techniques : an introduction

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Coherent beam combining of diode lasers:

WHY ?

WHAT ?

HOW ?

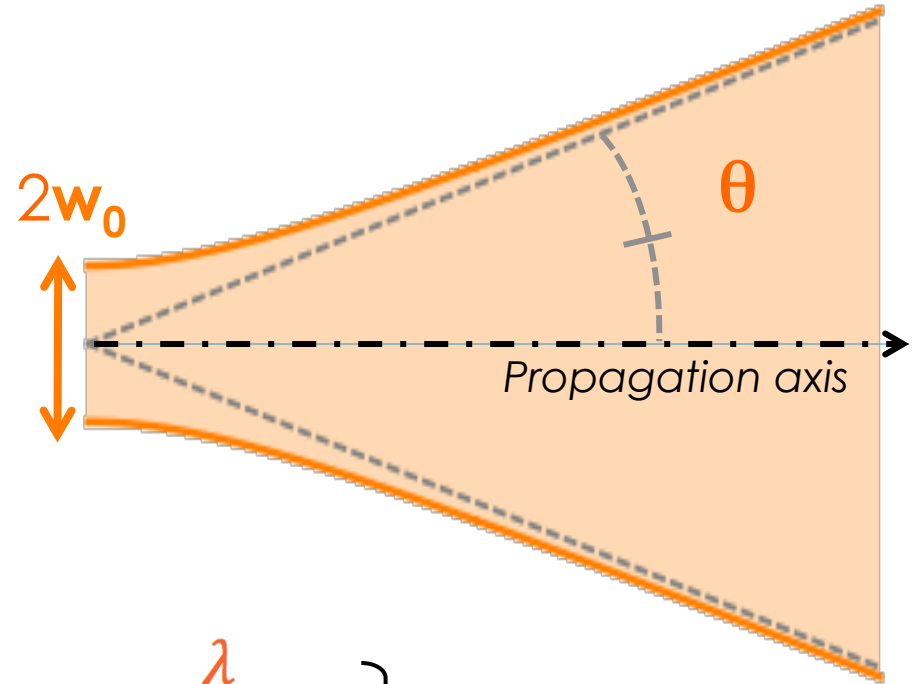
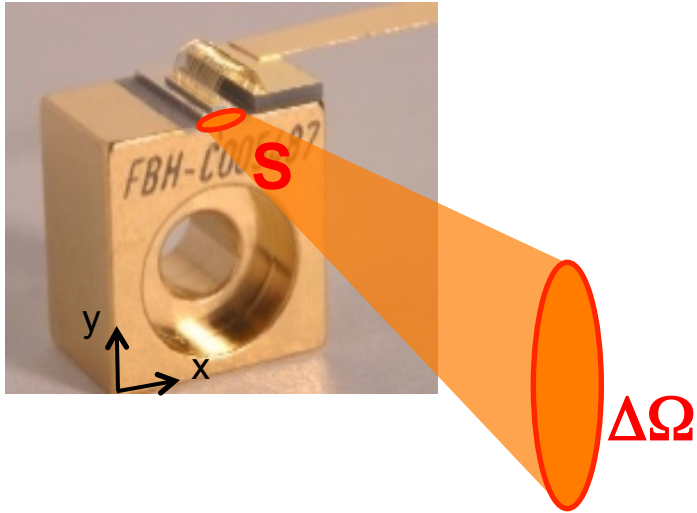
WARUM ?

WAS ?

WIE ?

Outline

- **Introduction**
 - brightness of a laser source
 - beam combining architectures
- **Coherent beam combining**
 - active MOPA configuration
 - self-organising external cavities



Gaussian diffraction-limited beam : $\theta = \frac{\lambda}{\pi w_0}$

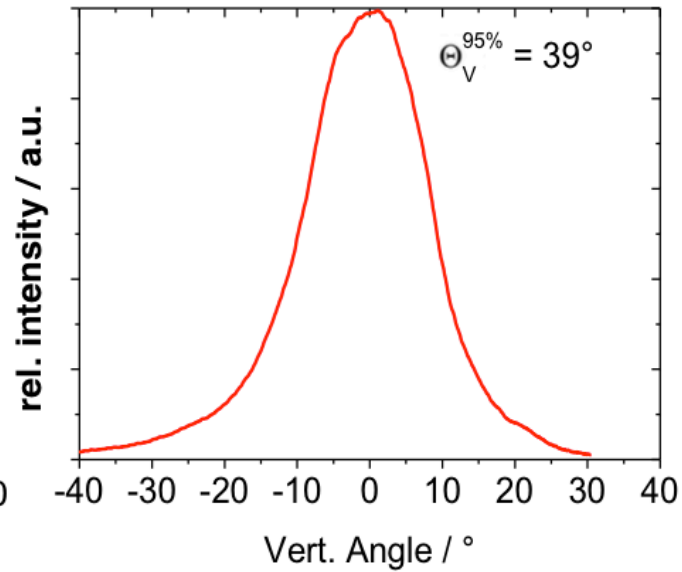
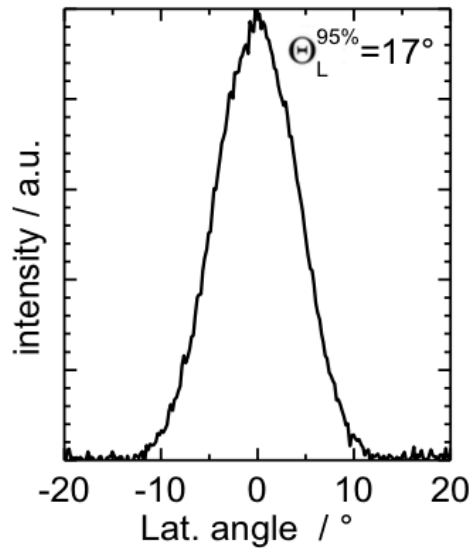
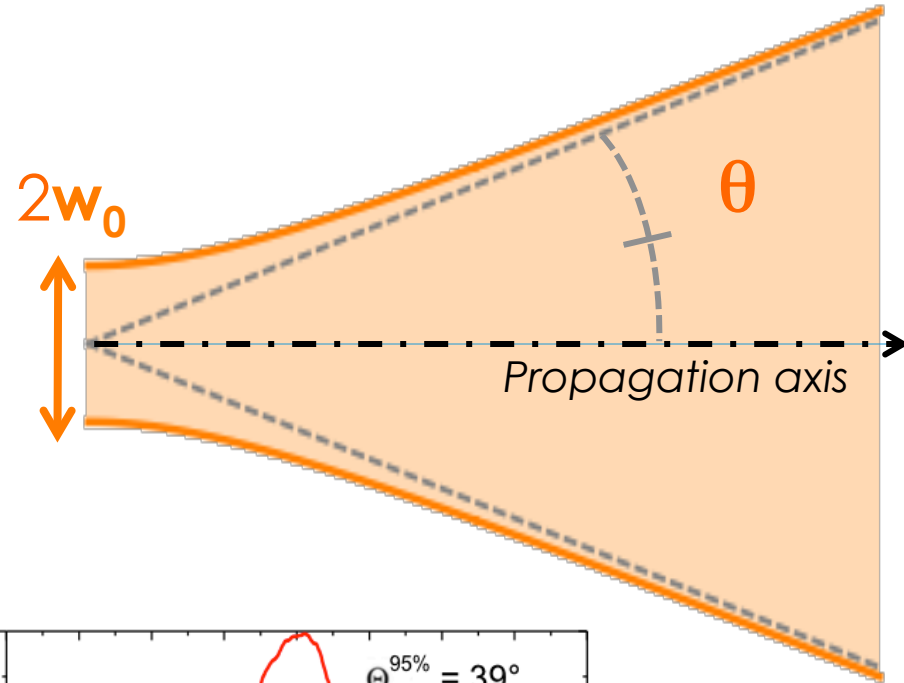
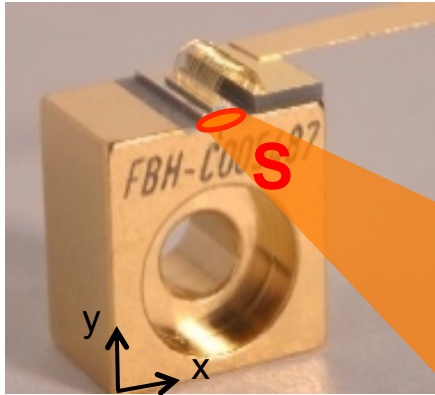
General case : $\theta = M^2 \times \frac{\lambda}{\pi w_0}$

Beam quality parameter

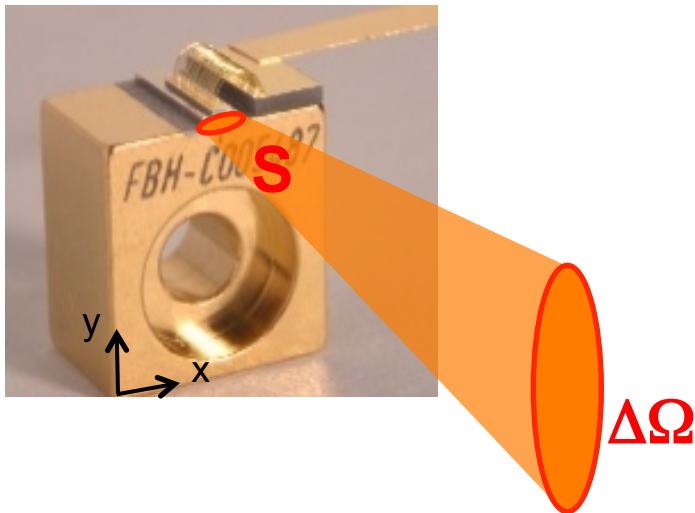
in both x/y axes

Beam parameter product : $BPP = \theta \times w_0 = M^2 \times \frac{\lambda}{\pi} \cong 0.3 \times M^2$ @ $\lambda = 1 \mu\text{m}$

Laser beam propagation : diode lasers



What is the brightness of a laser source ?



→ The brighter the better ...

Brightness = measurement of the power and beam quality of a laser source

$$B = \frac{P}{S_{em} \times \Delta\Omega} = \frac{P}{\lambda^2 \times M_x^2 M_y^2} \quad [\text{unit : W.m}^{-2}.\text{sr}^{-1}]$$

⇔ ability to focus a high power on a small area with a low NA

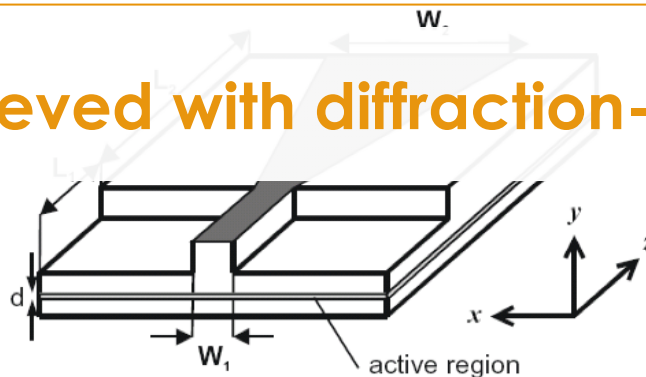
What is the brightness of a laser source ?

Brightness = measurement of the power and beam quality of a laser source

$$B = \frac{P}{\lambda^2 \times M_x^2 M_y^2}$$

State-of-the-art	Power	$M_x^2 \times M_y^2$	Brightness
Single-mode LD (a)	1 W	1	100 MW.cm ⁻² .sr ⁻¹
Broad area LD (b)	7 W	1 x 6	110 MW.cm ⁻² .sr ⁻¹
Tapered LD (c)	12 W	1 x 1.2	1000 MW.cm ⁻² .sr ⁻¹

Highest brightness achieved with diffraction-limited laser sources

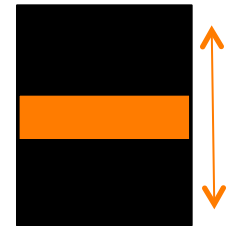


- (a) SCOWL – Donnelly *et al*, IEEE JQE 39, 2 (2003)
 (b) P. Crump, BRIDLE
 (c) Fiebig *et al*. Elec. Lett, 44, p1253 (2008)

- ↗ **output power** of single-mode devices
 - ⇒ increase the power density on facets
 - ⇒ damages & deterioration of lasers

$$B = \frac{P}{\lambda^2 \times M_x^2 M_y^2}$$

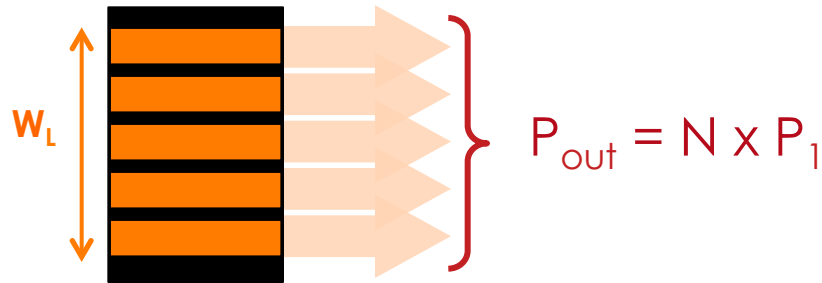
- ↗ **output power**
 - ⇒ increase the active volume
 - ⇒ **beam quality** ↘



- ↗ **output power** by **combining** parallel laser sources while maintaining the **beam quality**
- = beam combining



- Incoherent (*side-by-side*) combining

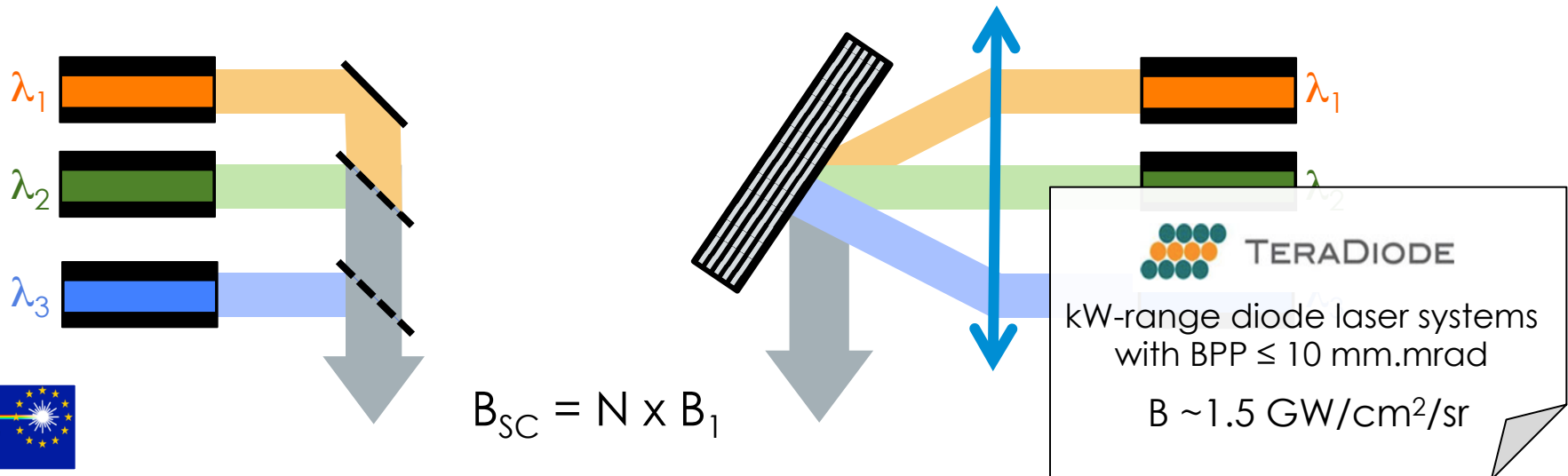


$\nearrow W_L$ but same divergence θ

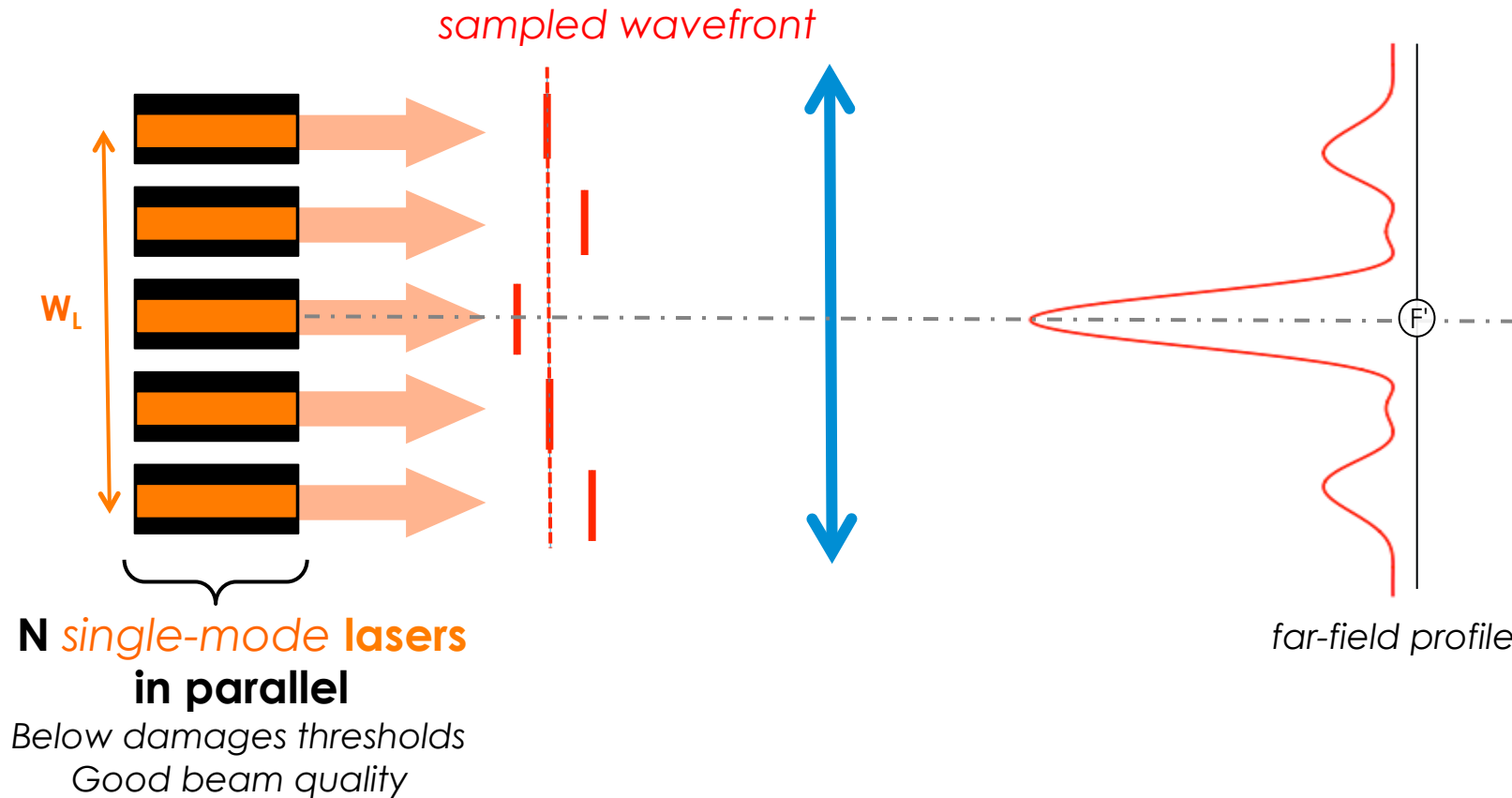
$$B_{bar} \leq B_1$$

- Spectral beam combining

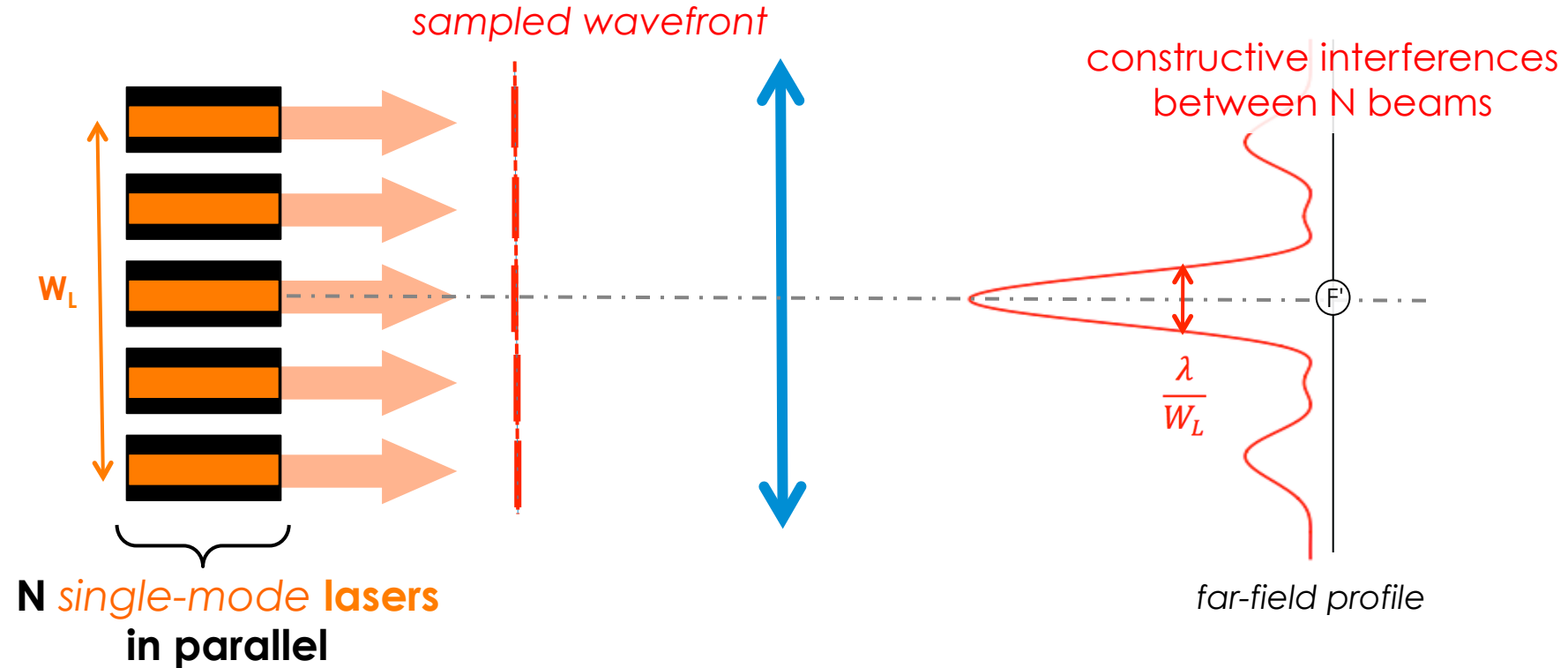
= superposition of \neq laser lines with grating / dichroïc mirrors / vol Bragg gratings



= **constructive superposition** of N laser beams with proper phase relationship



= **constructive superposition** of N laser beams with proper phase relationship

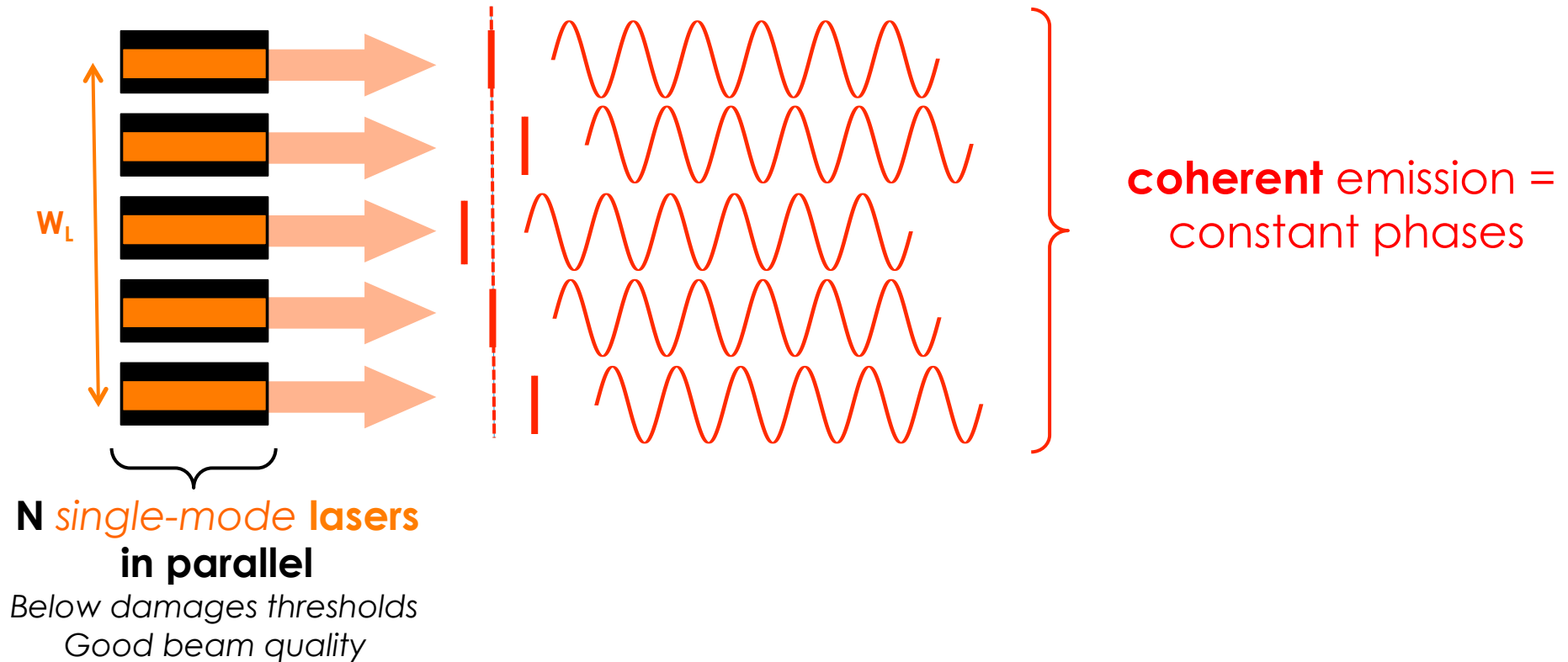


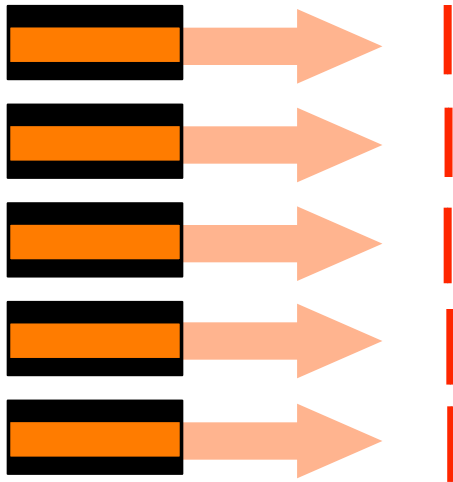
$$B_{CBC} = \frac{N \times P_1}{\lambda^2 \times M_x^2 M_y^2} = N \times B_{single}$$

\nearrow output power
 \nearrow emission width W_L & \searrow divergence θ

} \Rightarrow \nearrow **spatial brightness** + narrow $\Delta\lambda$

= **constructive superposition** of N laser beams with proper phase relationship



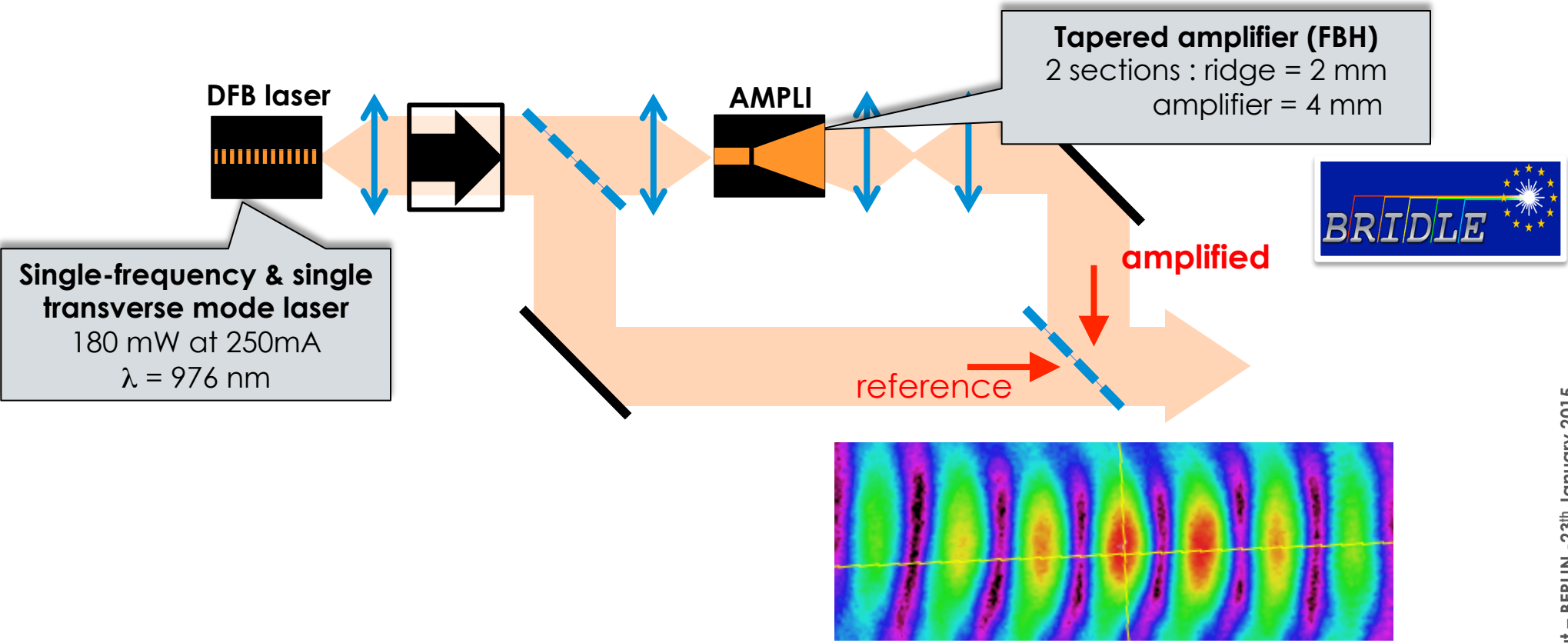


→ MOPA configuration
= **parallel amplification** of one seed
laser in N **amplifiers**

MOPA = Master Oscillator – Power Amplification

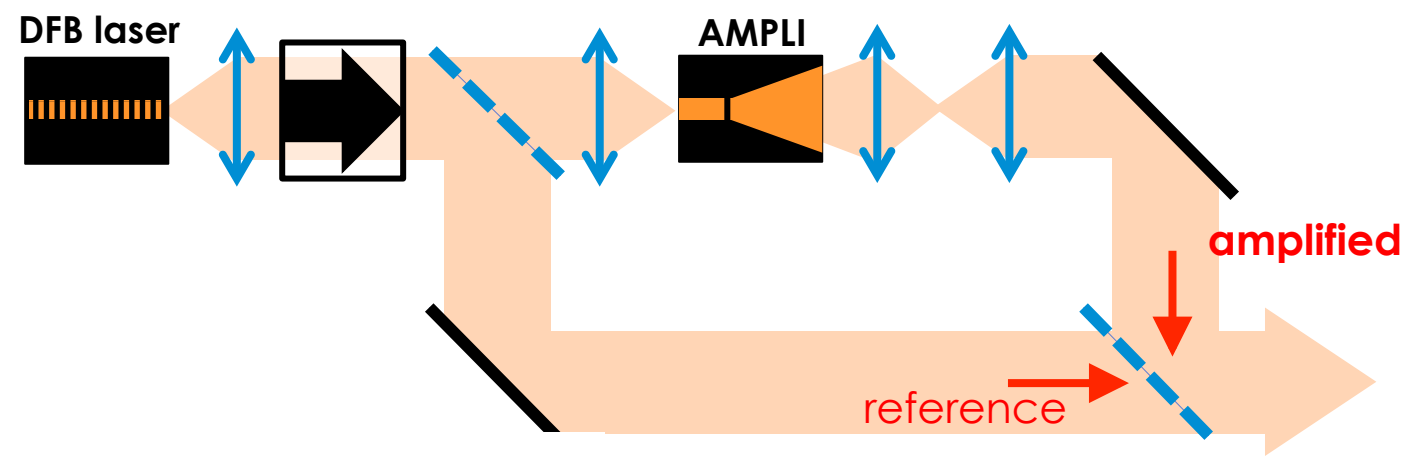
→ Self-organizing lasers
= spontaneous operation in the
phase-locked regime of N **lasers**

Demonstration of the amplification of a single-frequency laser beam in a tapered amplifier in a *Mach-Zehnder interferometer* configuration :



We observe highly-contrasted fringes on the combined port
 ⇒ the seed and amplified beams are phase-locked
 ⇒ the coherence between them is $\geq 96 \%$

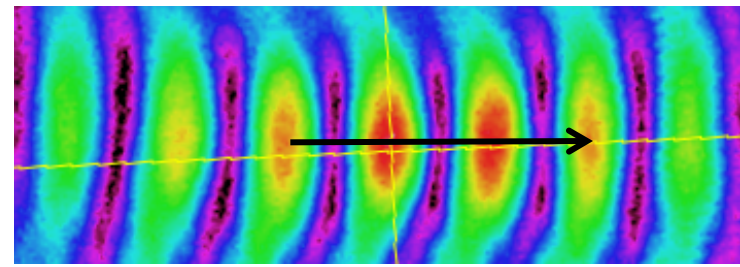
Demonstration of the amplification of a single-frequency laser beam in a tapered amplifier in a *Mach-Zehnder interferometer* configuration :



$$\varphi_{AMPLI}(I, T^\circ) = \frac{2\pi}{\lambda} n_{opt} L_{AMPLI}(I, T^\circ)$$

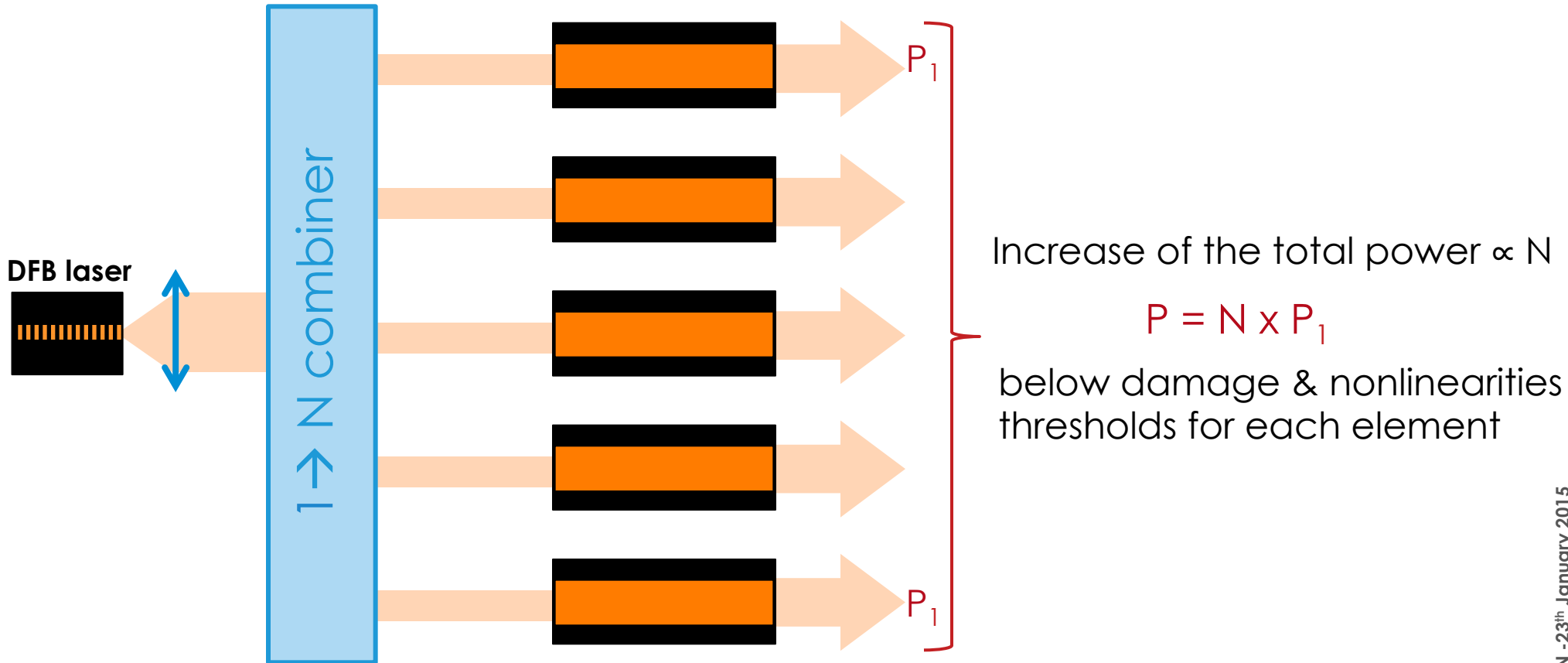
Phase-shift with ridge current

$$\frac{\Delta\varphi_{AMPLI}}{\Delta I_{ridge}} \cong 0.025 - 0.037 \pi/\text{mA}$$



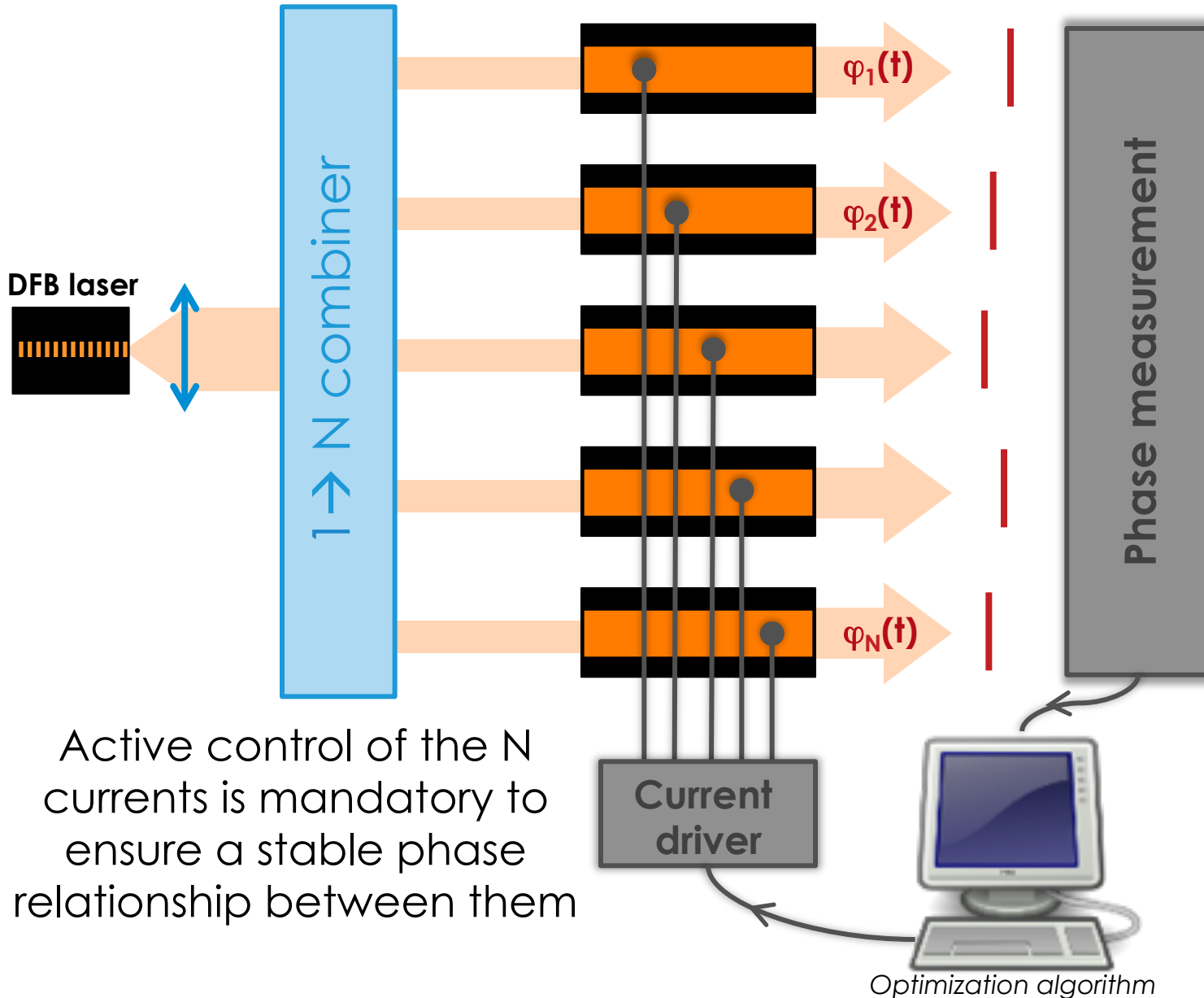
The fringes shift with the currents in the ridge & taper section, because of thermally-induced change of the optical path in the amplifier





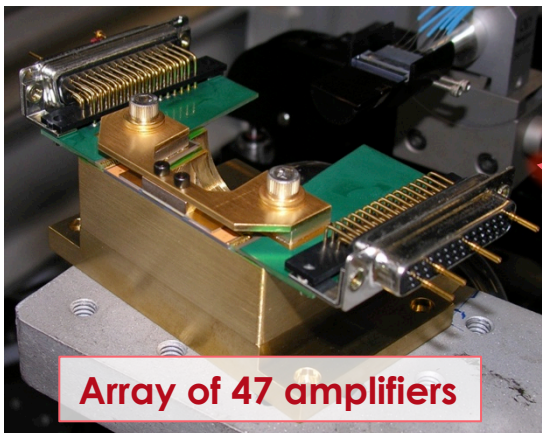
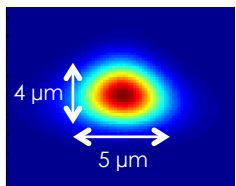
= Amplification of a single-frequency laser beam in multiple amplifiers in //

Phase-locking in a MOPA architecture

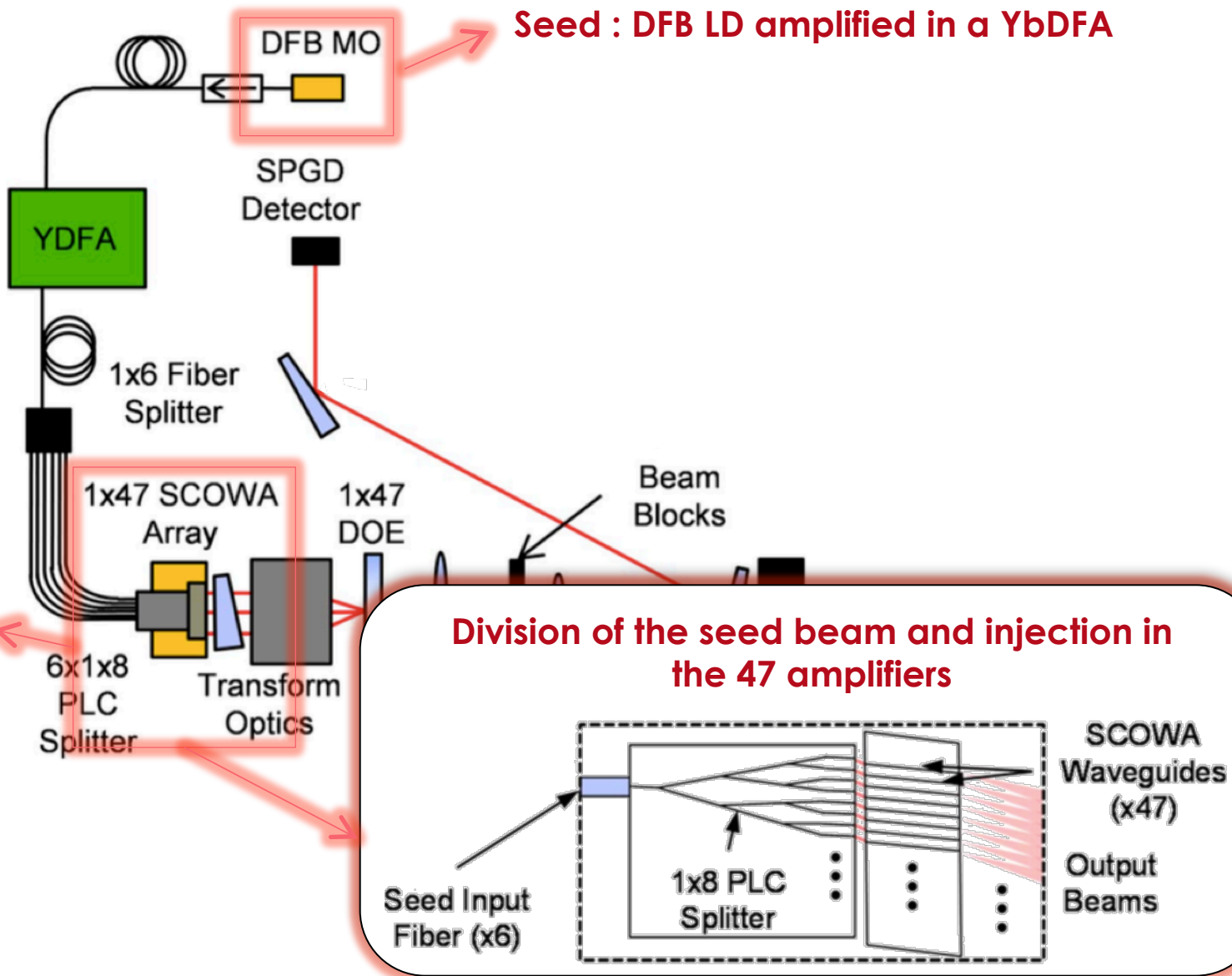


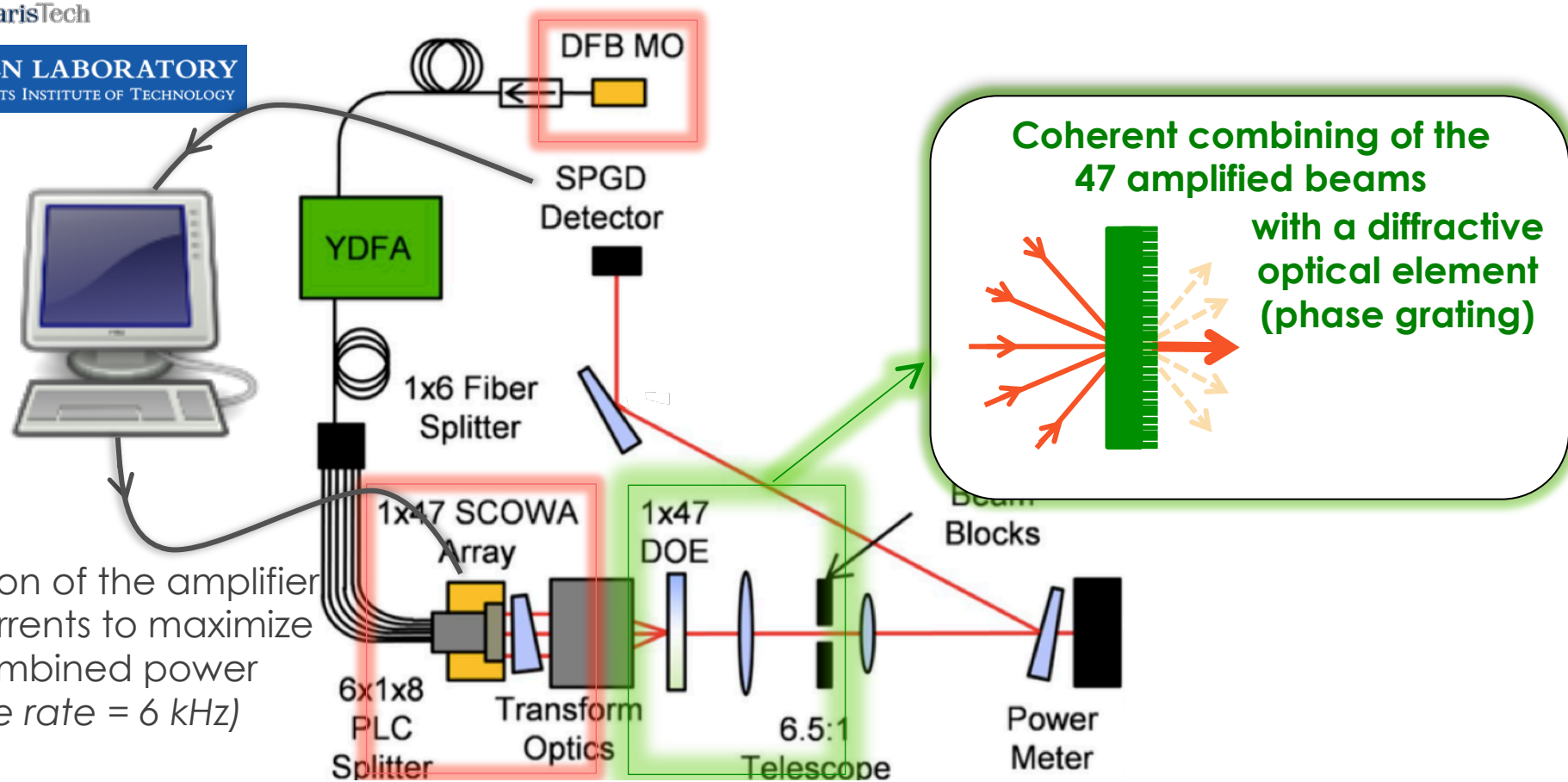
Active phase-locking of a SCOWL array

Single Element
Near Field



Array of 47 amplifiers





Optimization of the amplifier driving currents to maximize the combined power (update rate = 6 kHz)

→ Demonstration of the **active phase-locking & coherent beam combining** of 47 semiconductor amplifiers

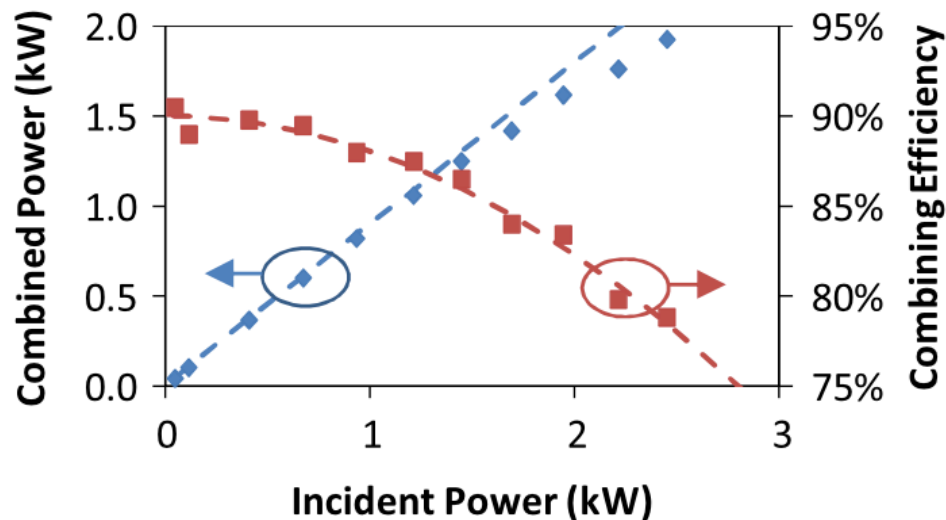
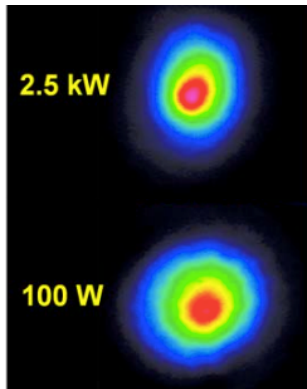
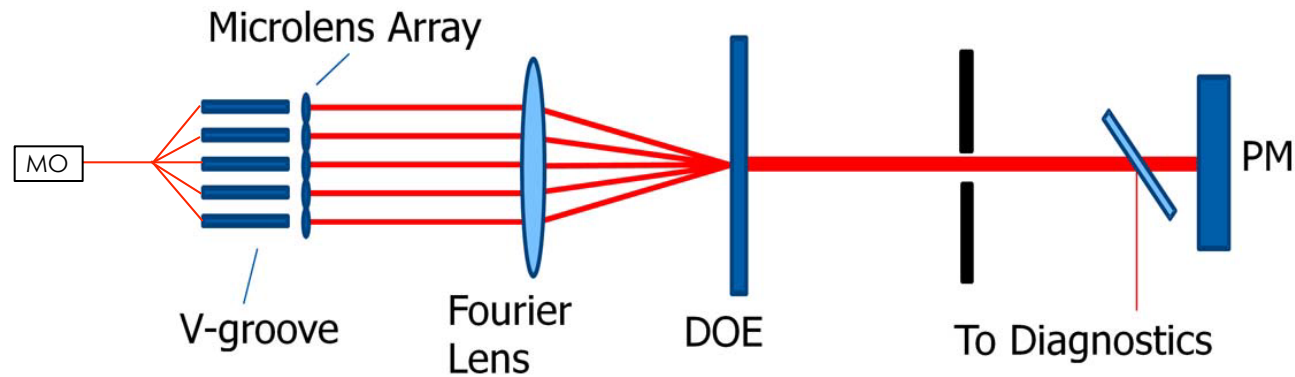
→ **Total output power = 40 W** with $\eta_{\text{CBC}} = 87\%$: $B \sim 2.5 \text{ GW.cm}^{-2}.\text{sr}^{-1}$

$$B_{\text{SC}} = 25 \times B_1$$

5 x 500 W Yb doped fibers amplifiers : **1.93 kW combined**

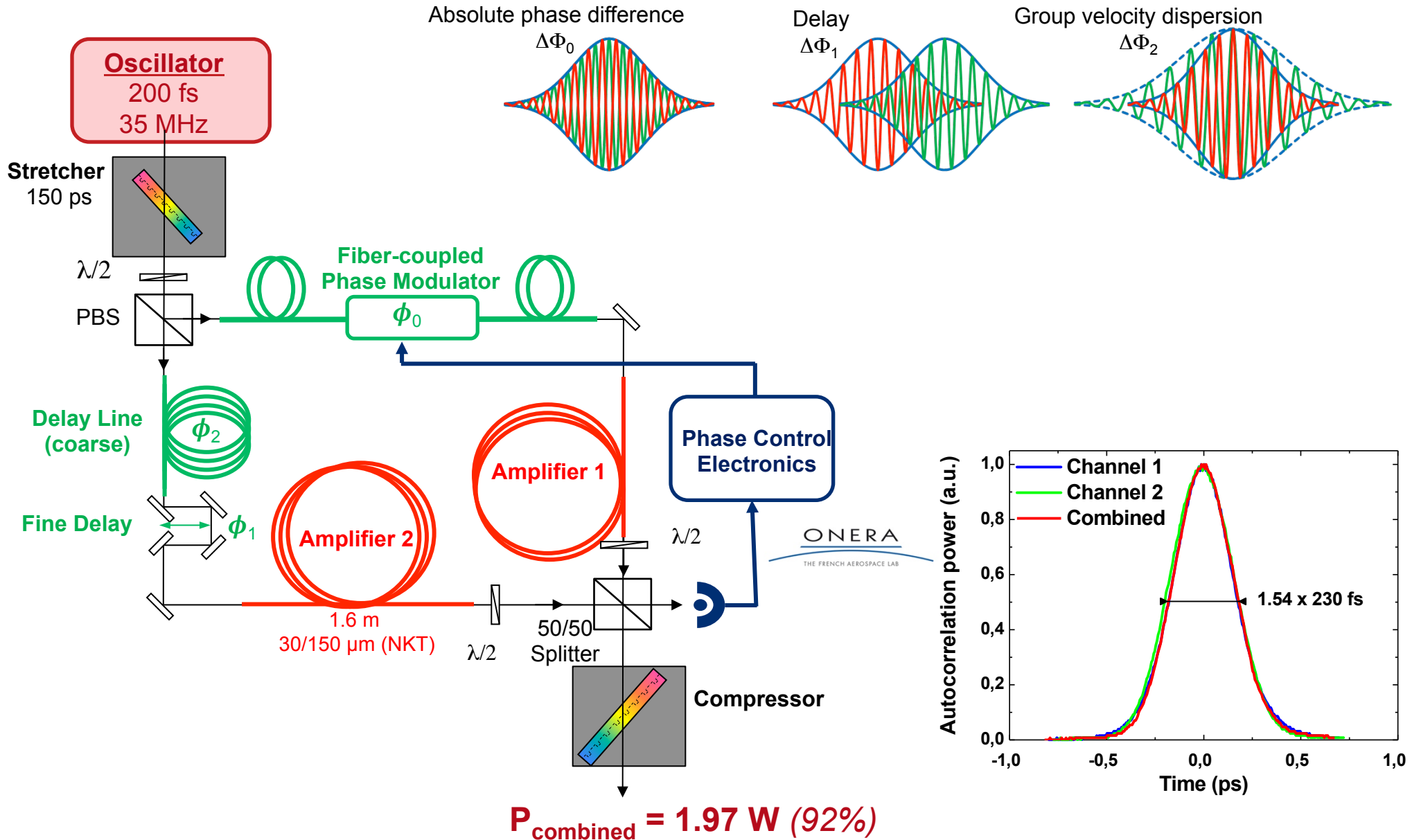
79 % efficiency, $M^2 = 1.1$

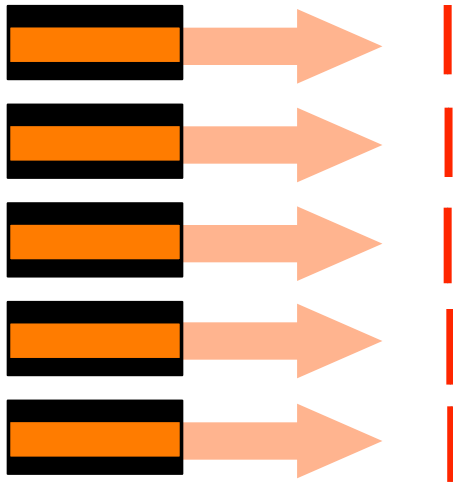
LOCSET active feedback



NORTHROP GRUMMAN

Massachusetts
Institute of
Technology





→ MOPA configuration
= **parallel amplification** of one seed laser in N amplifiers

→ Self-organizing lasers
= spontaneous operation in the phase-locked regime of N **lasers**

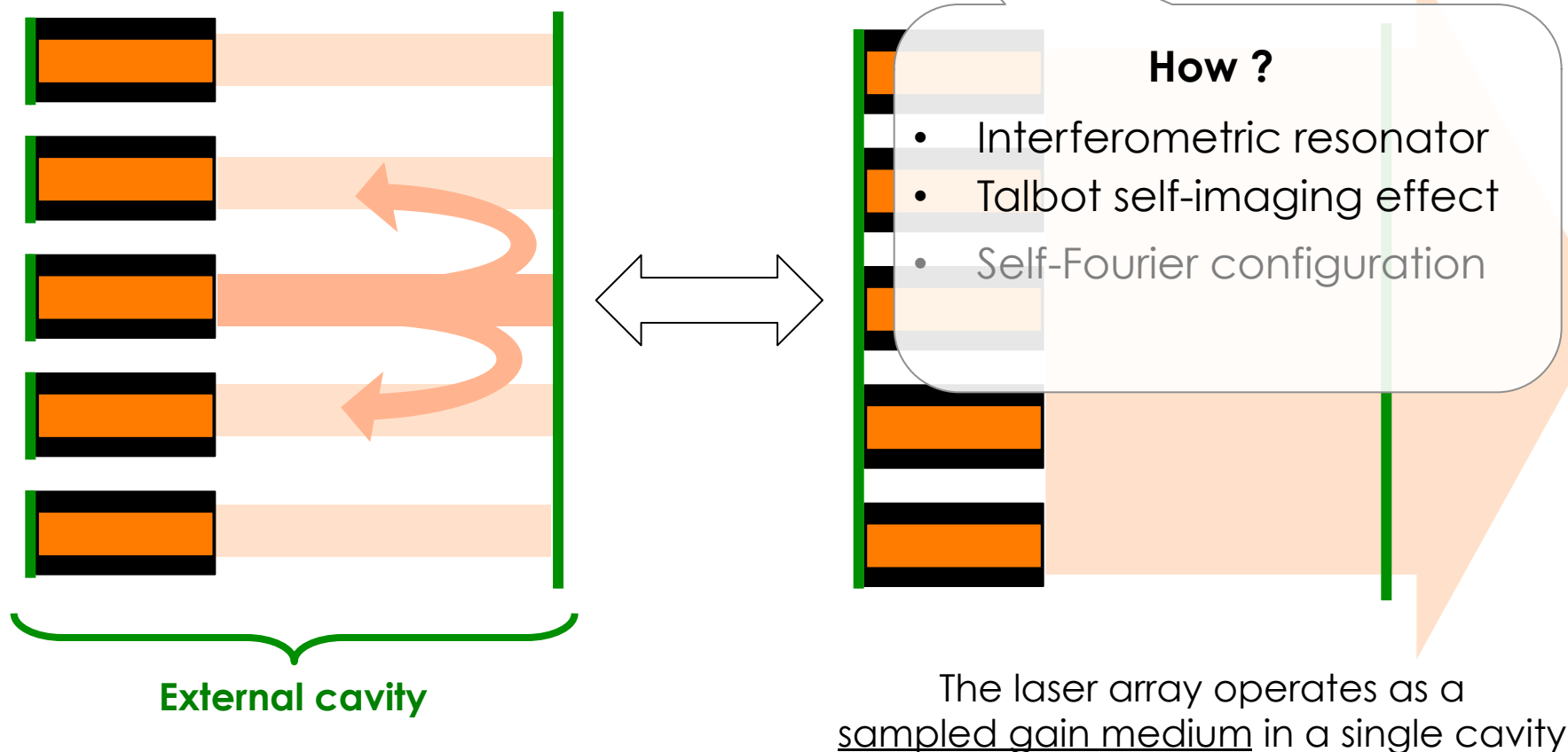
- phase-locked laser array
evanescent coupling between adjacent emitters

Diode Laser Arrays, ed. Botez & Scifres
(Cambridge Studies in Modern Optics)

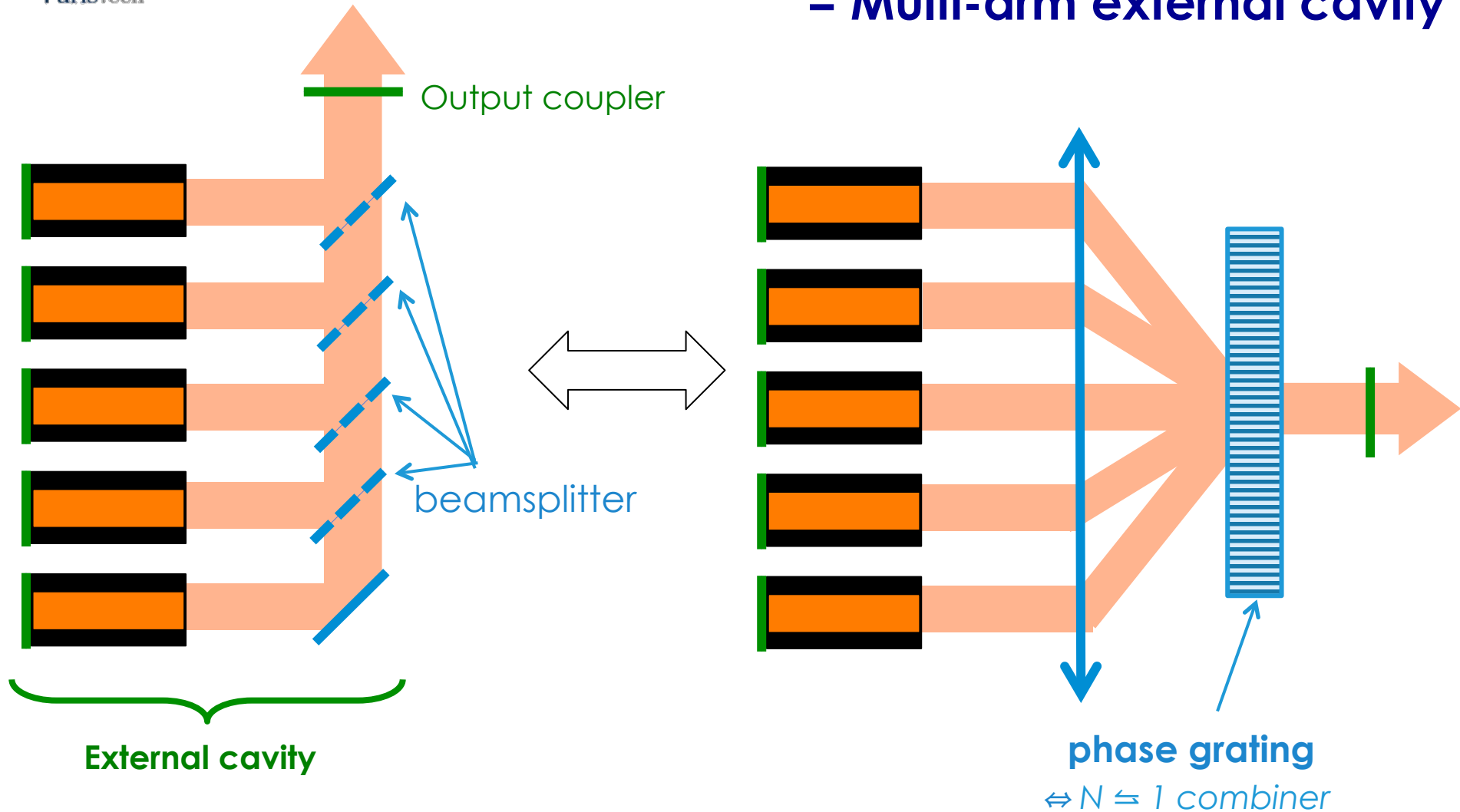
- lasers sharing a common external cavity

The external cavity is designed to favour the **collective operation** of the emitters by inducing a **coupling** between them.

⇔ *light from one emitter is reflected into the others*



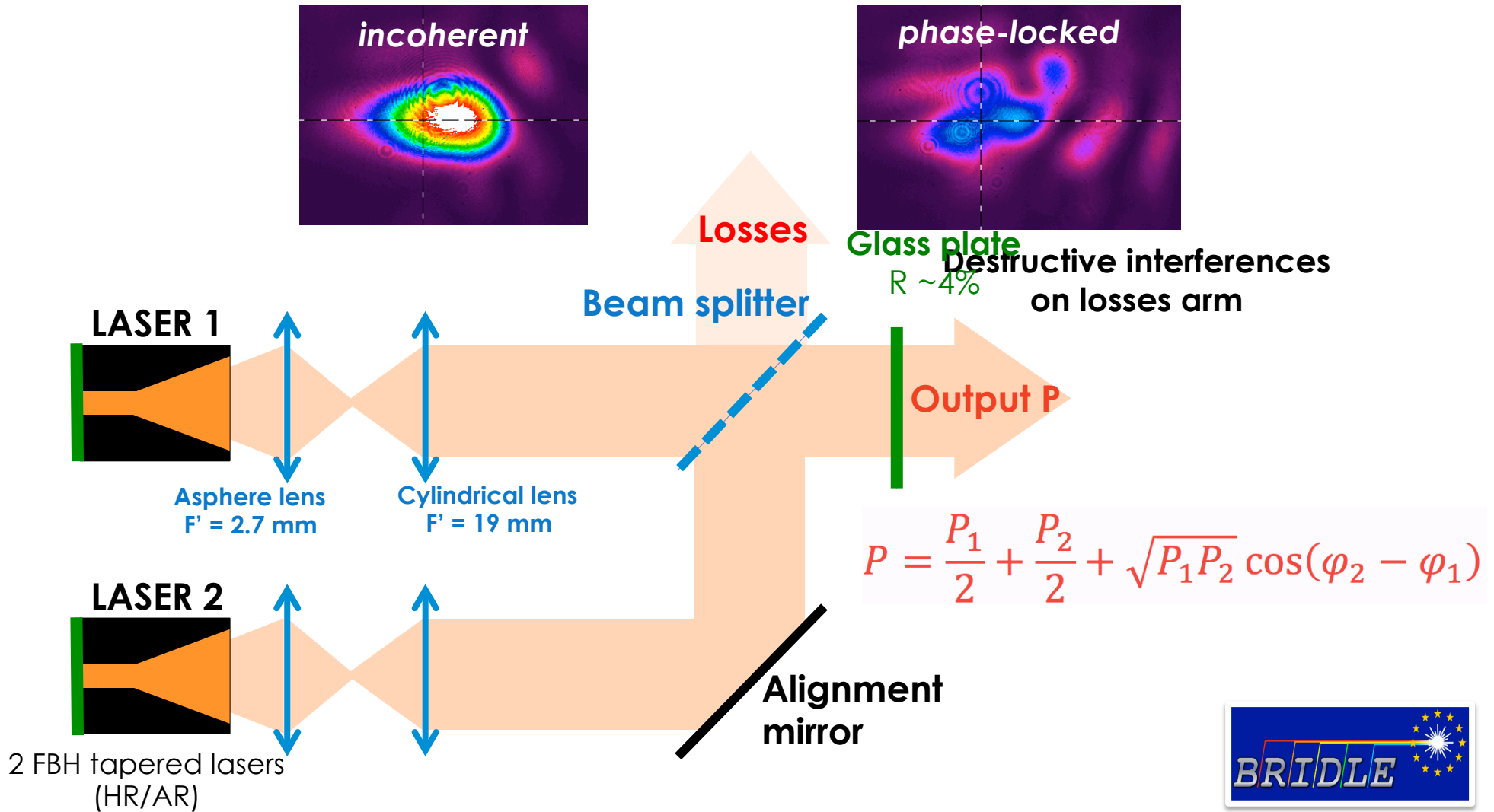
Interferometric resonator = Multi-arm external cavity

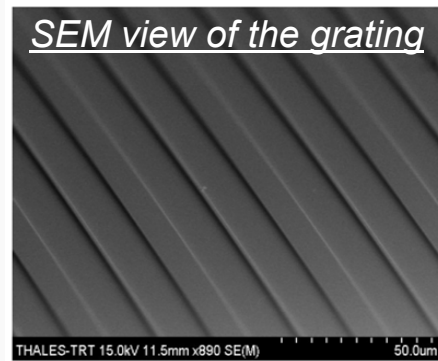
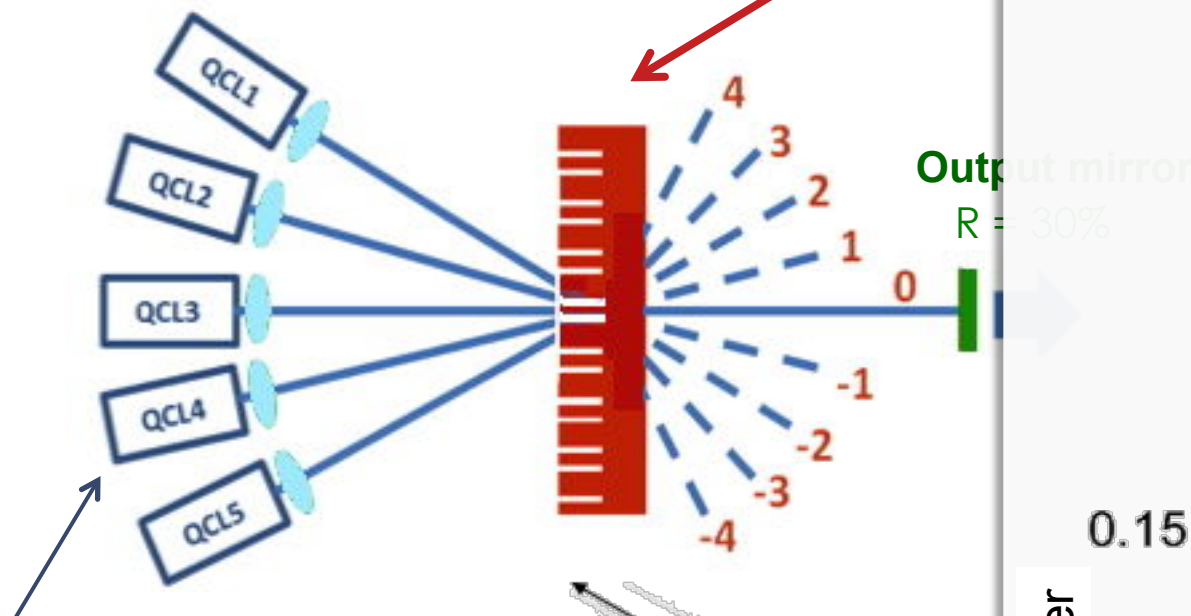


The external cavity favours constructive interferences between the multiple beams.

Michelson cavity : 2-arm interferometer

Minimum losses in the laser cavity for constructive interferences on BS in the P arm : **passive phase-locking** & **coherent combining** of the two lasers





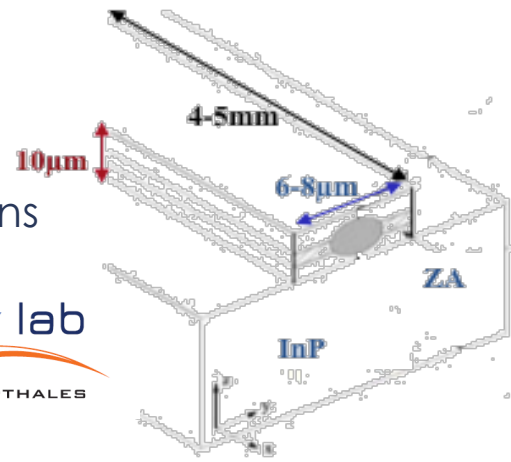
Binary phase grating ($0 - \pi$)
 $1 \cong 5$ combiner at $\lambda = 4.65 \mu\text{m}$
 Pitch $\Lambda = 50 \mu\text{m}$

Quantum Cascade Lasers

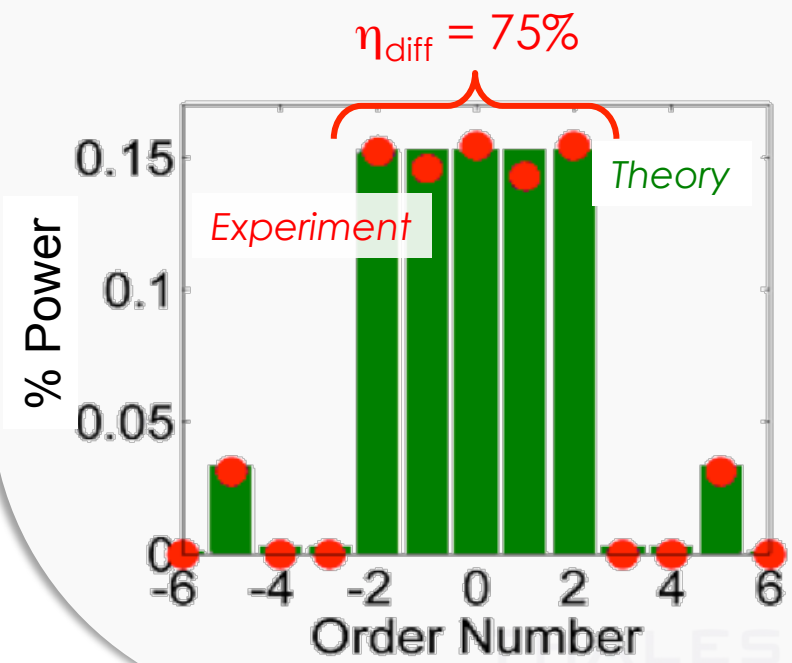
$\lambda = 4.6 \mu\text{m}$

GalnAs/AlInAs active regions
 HR / AR (<2%)

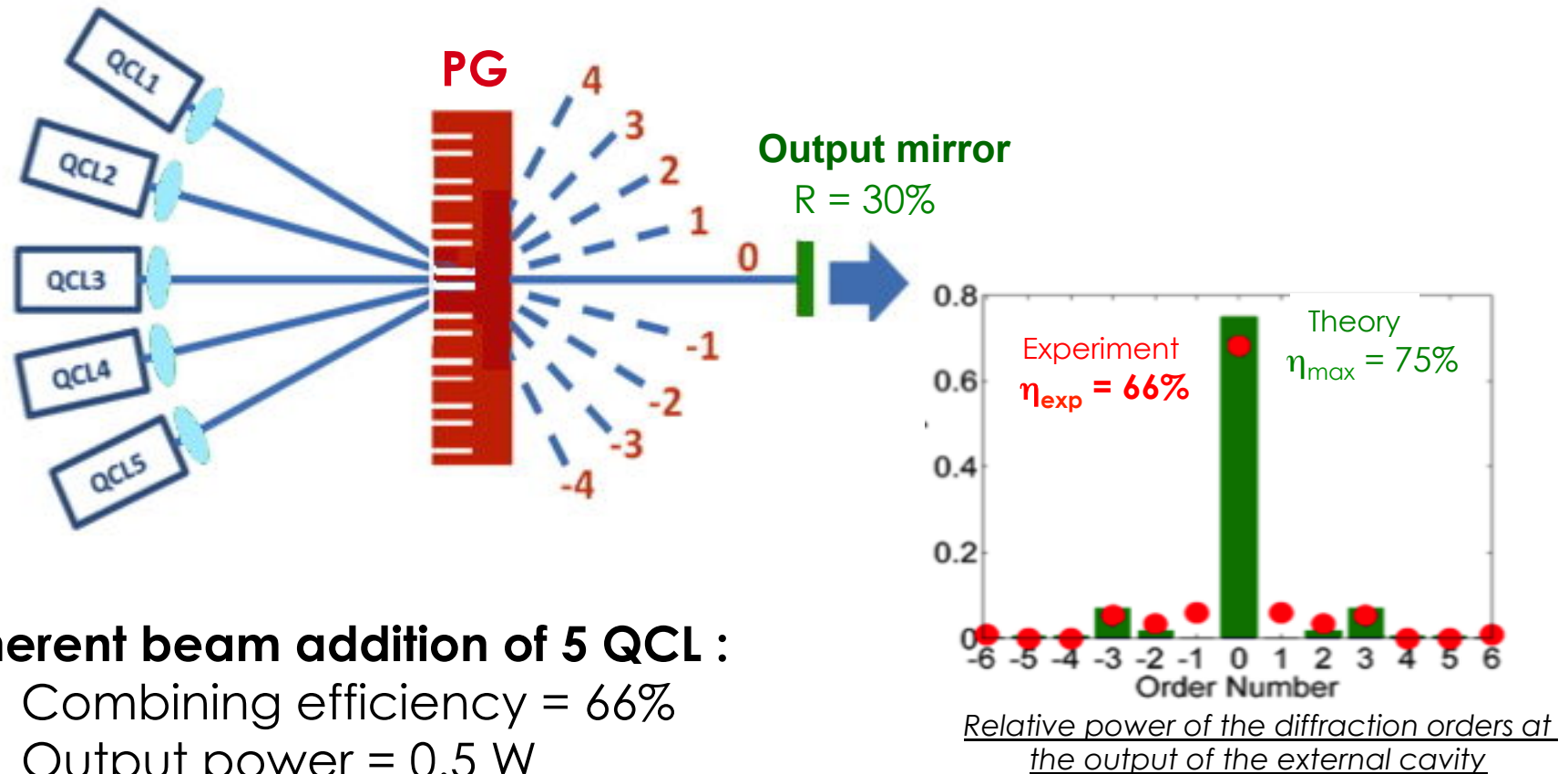
$M^2_y \leq 1.2, M^2_z \leq 1.5$



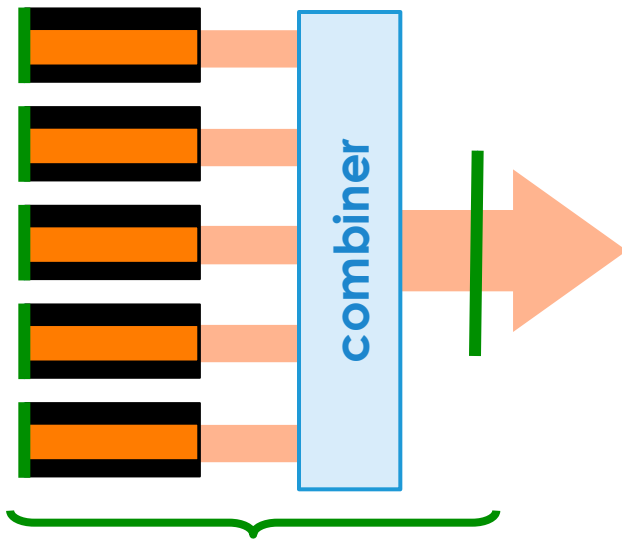
Phase grating



Minimum losses in the laser cavity for constructive interferences in the 0th order of the PG : **passive phase-locking & coherent combining**



→ **Coherent beam addition of 5 QCL :**
 Combining efficiency = 66%
 Output power = 0.5 W
 Diffraction-limited beam ($M^2 < 1.6$)



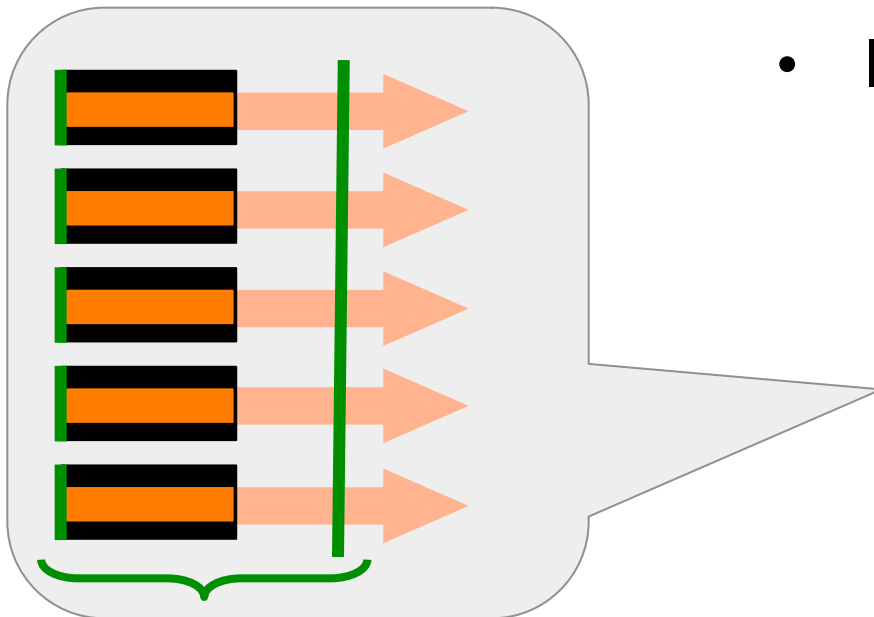
→ MOPA configuration
= **parallel amplification** of one seed laser in N amplifiers

→ Self-organizing lasers
= spontaneous operation in the phase-locked regime of N **lasers**

- lasers in a **common external cavity**

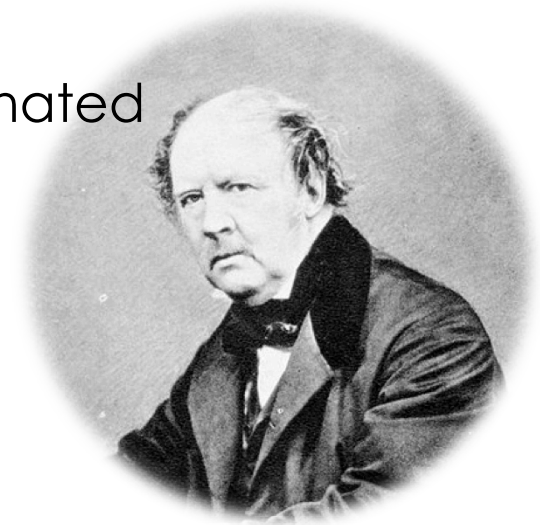
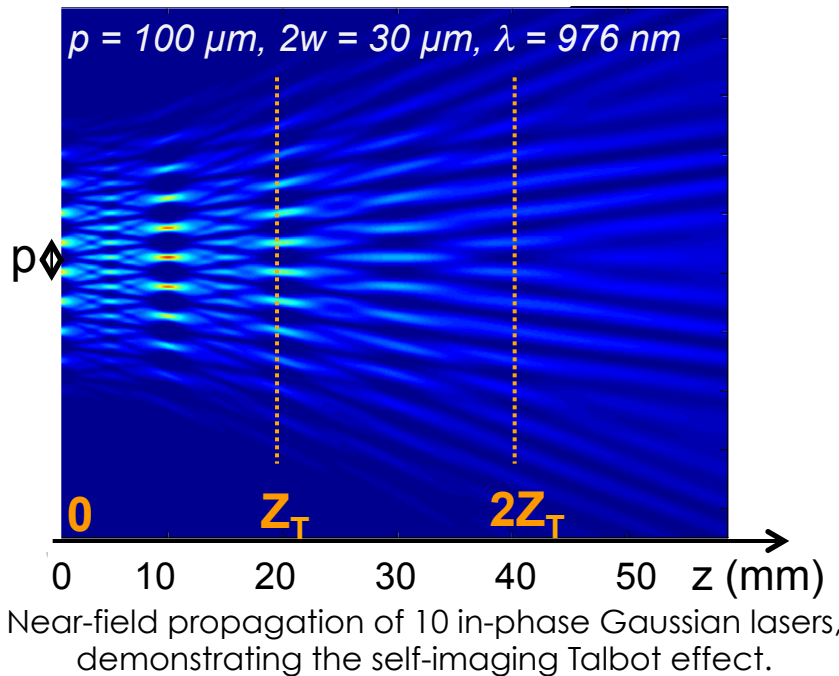
Interferometric resonator
⇒ *filled aperture*

Self-imaging cavity : Talbot effect
⇒ *tiled aperture*

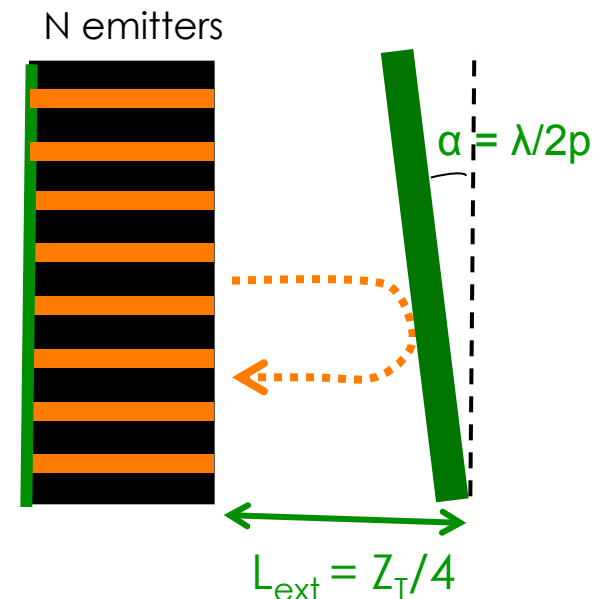


Near-field diffraction effect observed for a grating illuminated by monochromatic light :

→ self-images (E, φ) at multiples of $\frac{Z_T}{2} = \frac{p^2}{\lambda}$

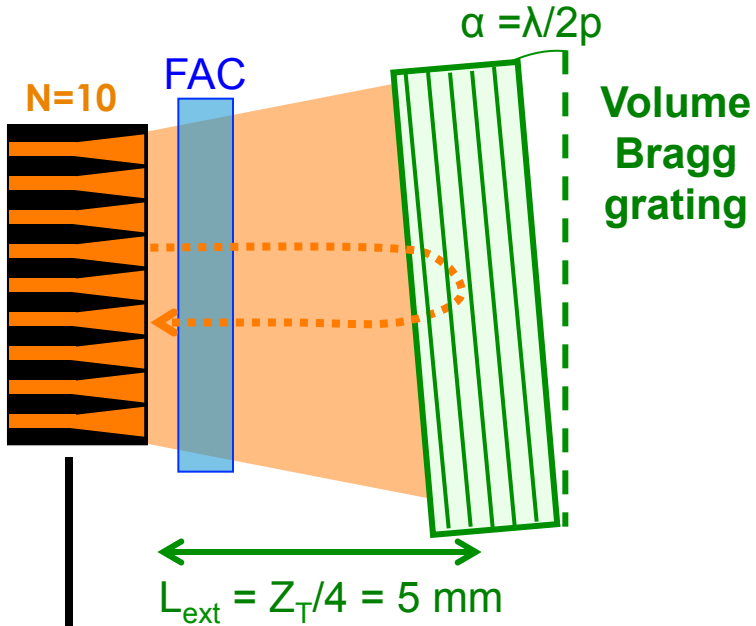


W. H. F. Talbot
"Facts relating to optical science"
Philos. Mag. 9 (1836)



⇒ effect used in an external cavity to maximize the coupling between emitters :
maximum back reflection of light for $L_{\text{ext}} = Z_T/4$

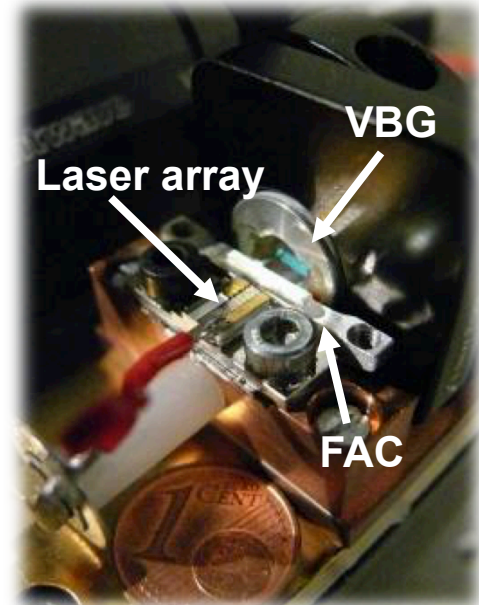
Passive phase-locking in a Talbot cavity



→ Output coupler with angular + spectral selectivity

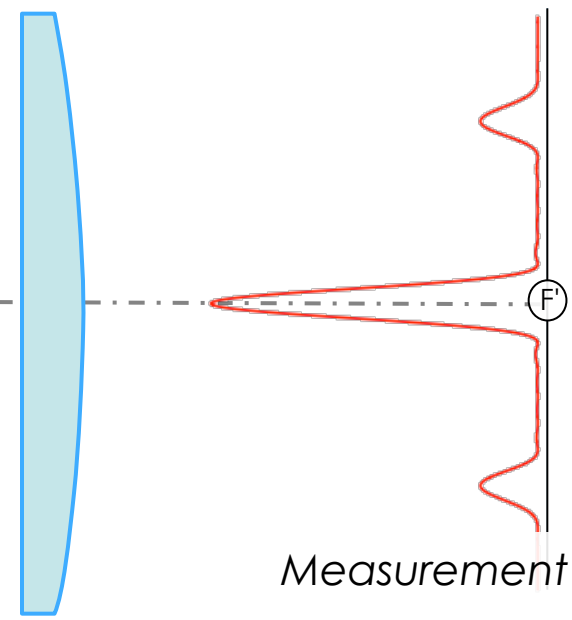
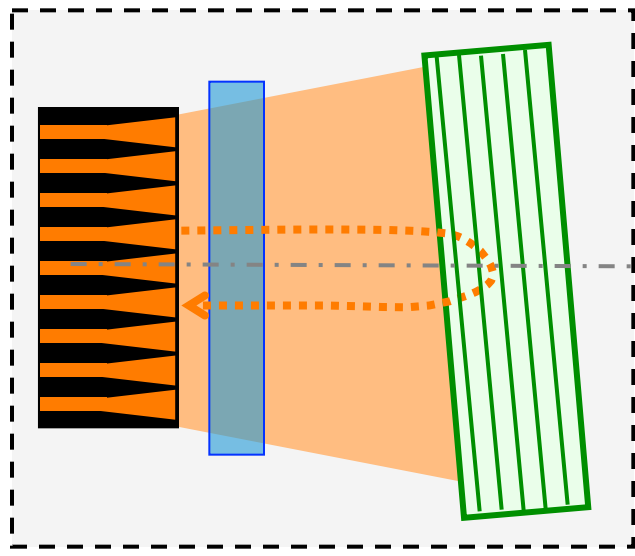
$R_B \cong 40 \%$
 $\lambda_B = 975.4 \text{ nm}, \Delta\lambda = 0.3 \text{ nm}$
 $\Delta\theta = 2^\circ \text{ (FWHM)}$

Array of 10 index-guided tapered emitters
 pitch = 100 μm , 0.4W/emitter

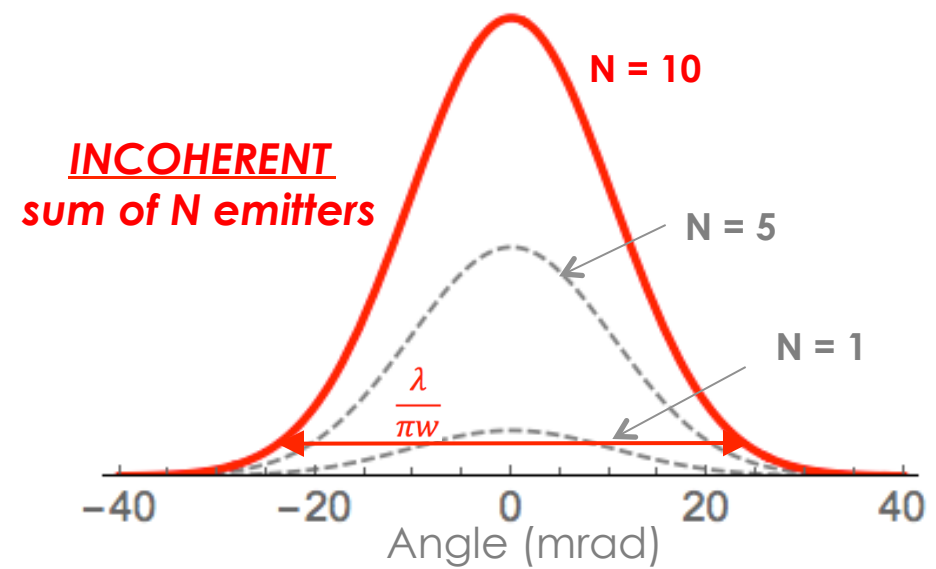


Experimental setup

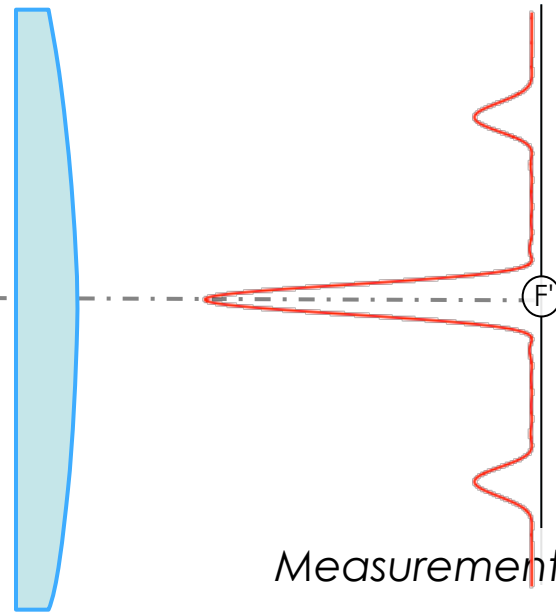
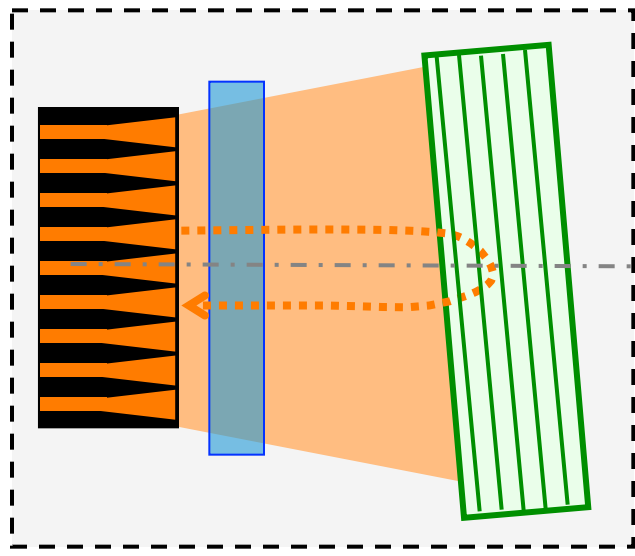
Evaluation of the coherence of the array



Measurement of the far-field profile



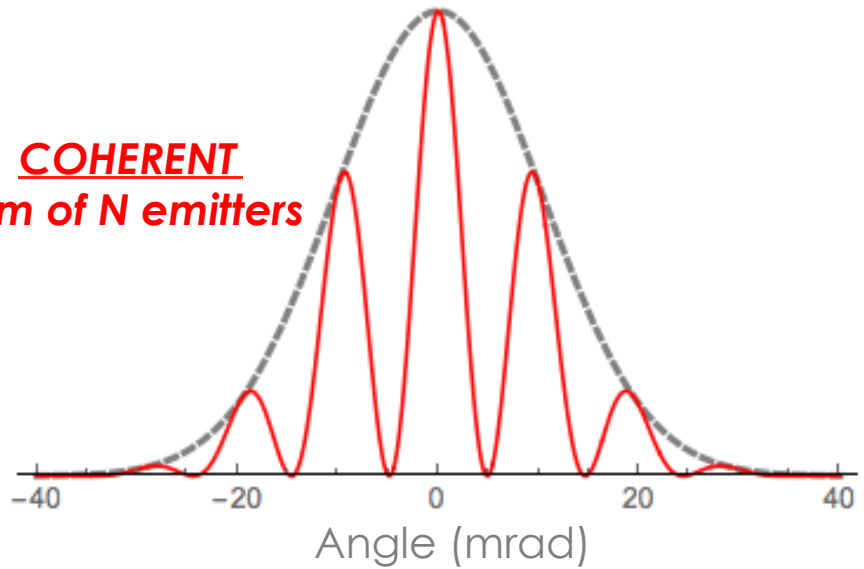
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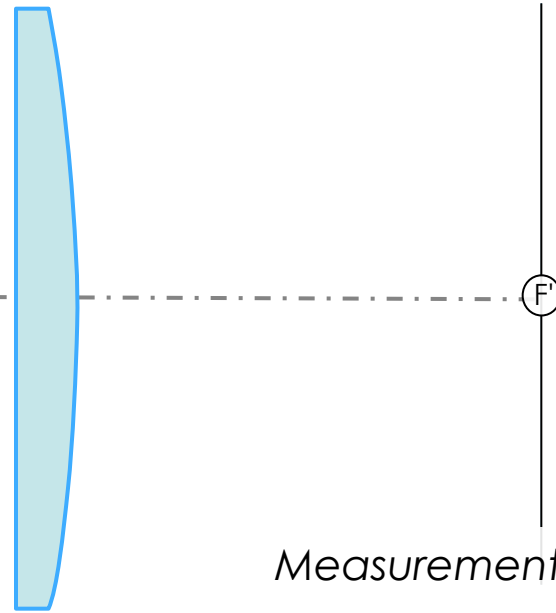
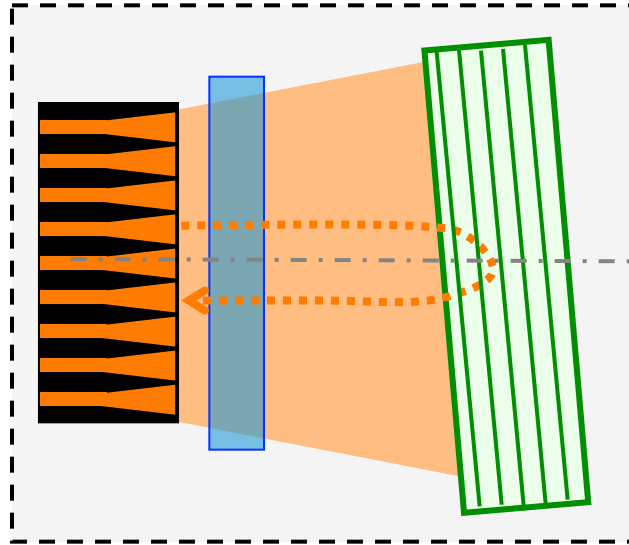


Measurement of the far-field profile

N = 2 in-phase emitters

COHERENT
sum of N emitters

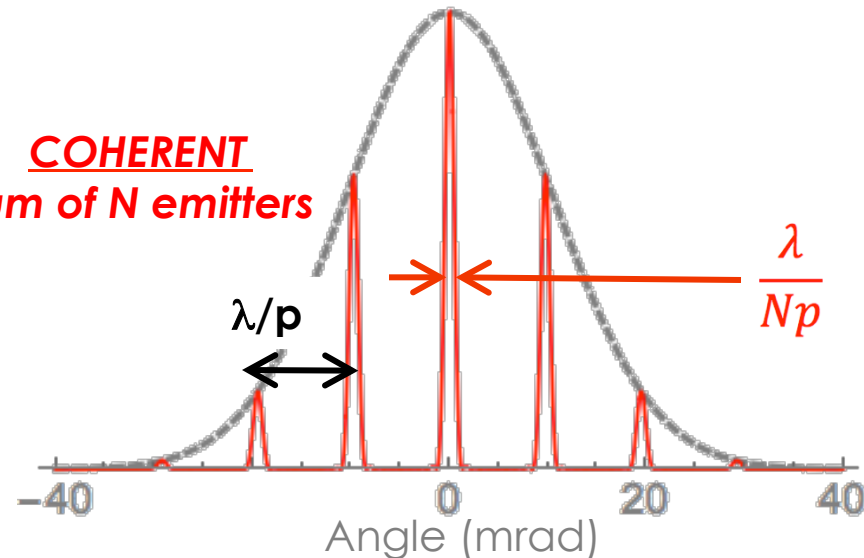




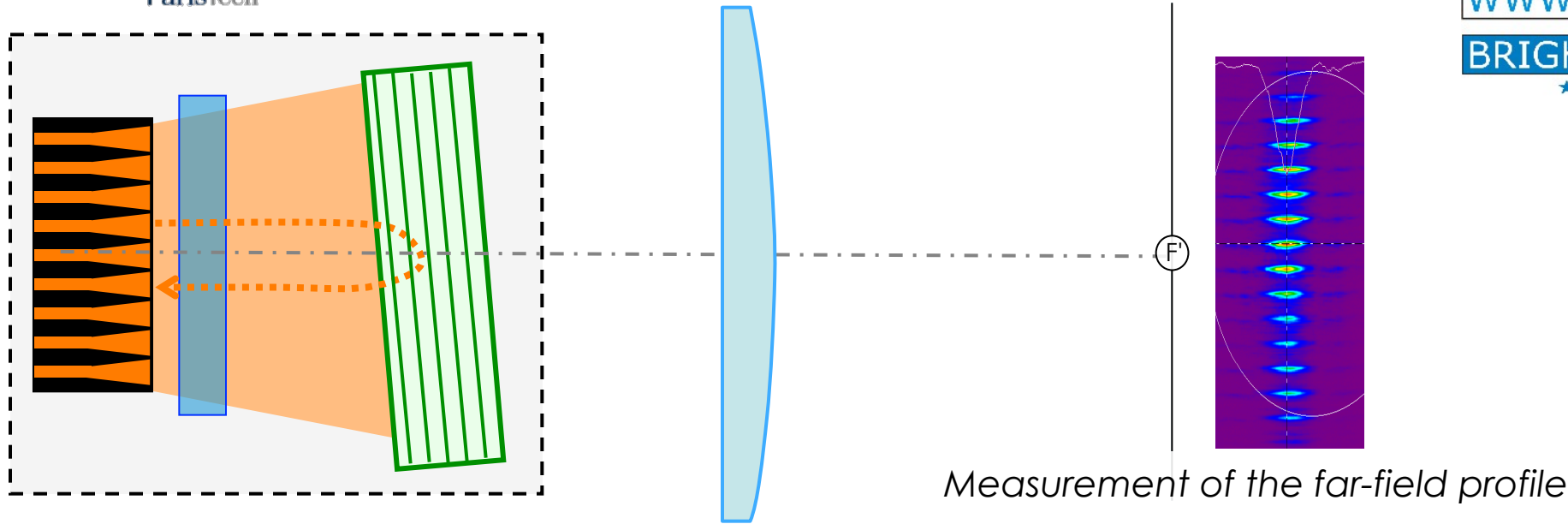
Measurement of the far-field profile

N = 10 in-phase emitters

**COHERENT
sum of N emitters**



→ Coherent operation is evidenced by
regularly spaced
& narrow peaks
in the FF profile

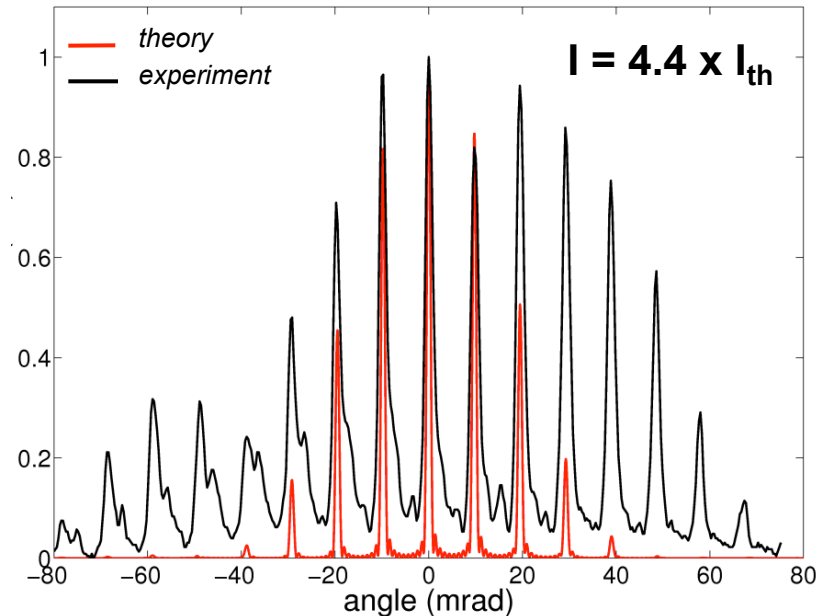


Measurement of the far-field profile

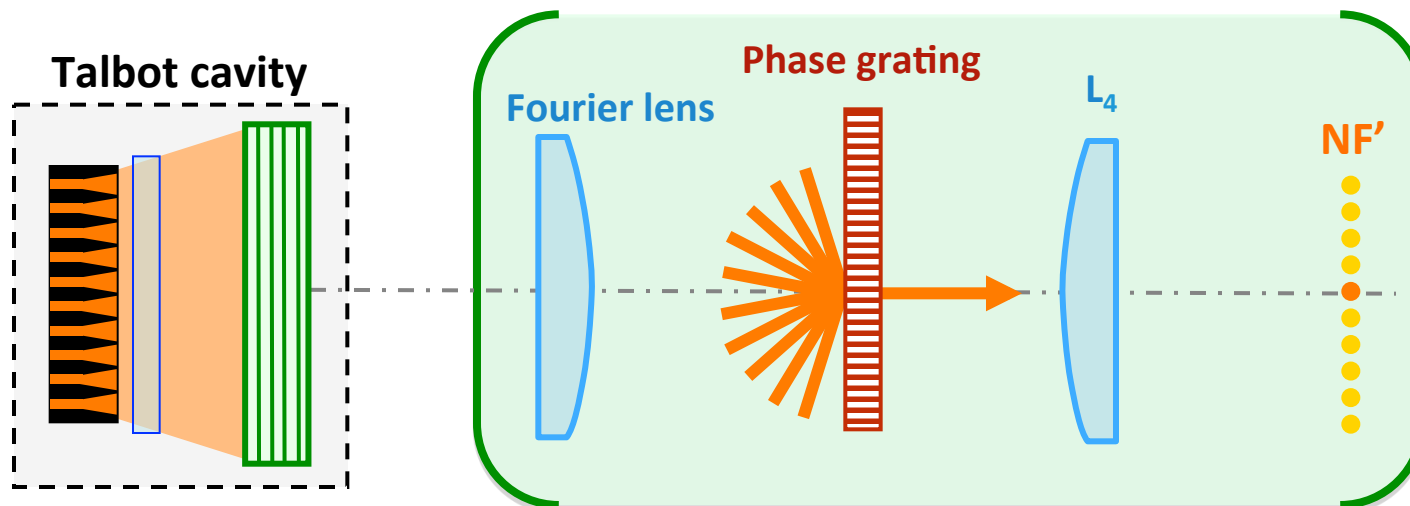
Spectral locking of each laser diodes
Narrow linewidth ($\Delta\lambda < 0.1 \text{ nm}$)

Laser threshold $I_{th} = 0.9 \text{ A}$
 $P_{max} = 1.7 \text{ W} @ 4 \text{ A} (4 \times I_{th})$

Operation in the in-phase mode
Highly-contrasted fringes in the FF
 $V \geq 80\%$



Near-field conversion setup

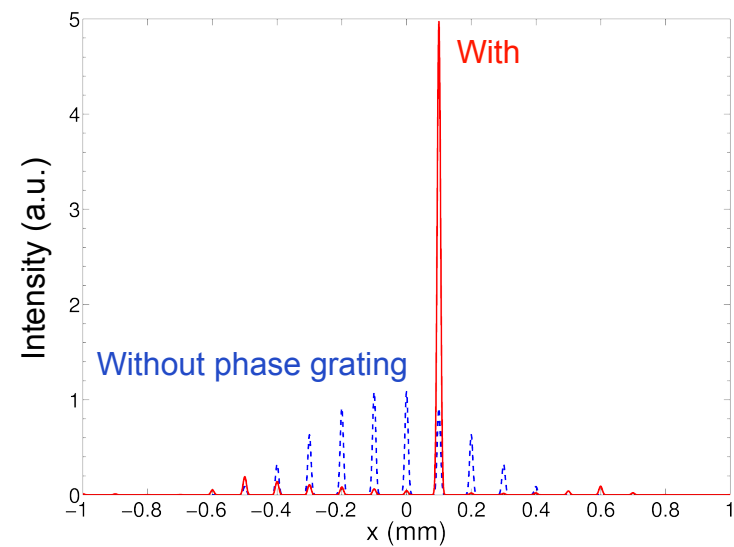


- Passive **phase-locking** of diode lasers in the Talbot external cavity
- + Passive **conversion** of the complex pattern in a Gaussian-like mode

Diffraction of the $N = 10$ coherent beams on a phase grating within 1 direction

⇒ **coherent superposition** of the emitters in the near-field plane NF'

Experimental superposition efficiency $\leq 51\%$



→ MOPA configuration

= **parallel amplification** of one seed laser in N **amplifiers**

Active electronic feedback

Linear phase-shift with control

→ Self-organizing lasers

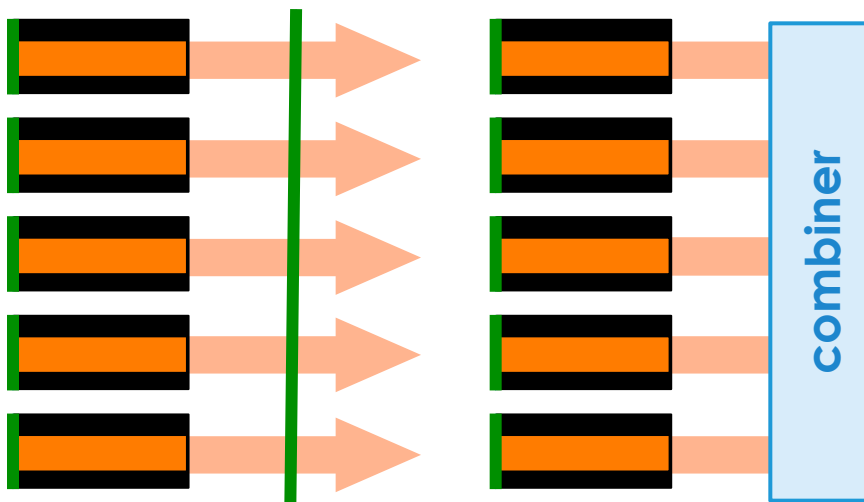
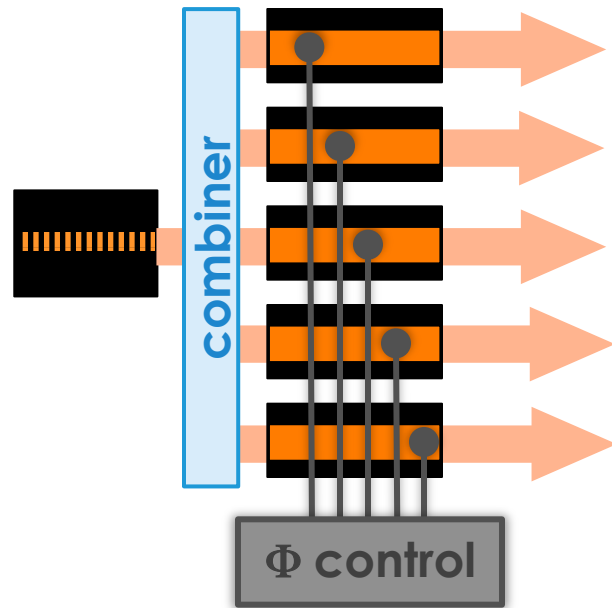
= spontaneous operation in the phase-locked regime of N **lasers**
lasers in a **common external cavity**

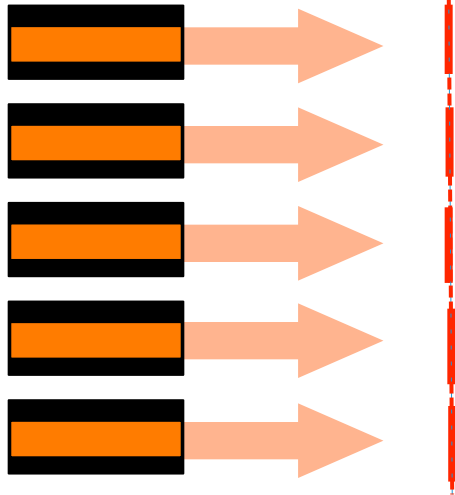
Interferometric resonator

Self-imaging cavity

Passive optical feedback

Highly non-linear behavior





- New interest in coherent beam combining techniques in the laser community (fiber, solid-state, diodes ...)
- Better understanding of the limits
- High-brightness CBC laser sources have been demonstrated
- Scaling to large number of emitters is still challenging.
- Active vs passive ? Electronic vs optic ?
- Detailed analysis of the physics of passively phase-locked lasers still needed.
- Careful design & optimization of the CBC architecture in regard with the devices.
- New results in BRIDLE expected !



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