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Passive coherent beam combining of quantum-cascade lasers with a Dammann grating

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An external cavity using a binary phase grating has been developed to achieve coherent combining of five quantum-cascade laser diodes, emitting at 4.65 μm. The combining of the five emitters is achieved by a binary phase grating or Dammann grating (DG) [8]. Multilevel phase gratings or continuous phase gratings present a higher efficiency, but are far more difficult to fabricate.

In order to prevent emission of the emitters alone in CW operation and thus to facilitate their phase-locking in the external cavity, their output facets were coated with an anti-reflection (AR) coating made of two layers of SiO2 and TiO2 (R < 2%).

The experimental setup is presented in Fig. 1. The external cavity extends between the rear facet of the five QCLs and the output coupler (OC). The OC is a GaAs plate presenting around 30% of Fresnel reflection with its rear facet AR coated (R ~ 2%). Because of their high divergence angle the QCLs are individually collimated with AR coated high aperture collimation lenses (CL) from LightPath (NA = 0.86, f = 1.88 mm). Two gold mirrors were added in each arm to align the five beams with respect to the DG orders. Because of their intersubband lasing transition, the output emission of QCL is linearly polarized along the normal direction to the layers of the active region. This well-defined polarization will ensure that the polarization states of the five emitters can easily be made parallel which is essential for coherent coupling.

The combining of the five emitters is achieved by a binary phase grating or Dammann grating (DG) [8]. Multilevel phase gratings or continuous phase gratings present a higher efficiency, but are far more difficult to fabricate. The binary phase profile is optimized so that the grating is able to separate an incident beam at 4.65 μm with a linear polarization parallel to the grooves into five beams of equal intensities with a good splitting efficiency (defined as the ratio of the power in the five central orders).
to the incident power). The five QCLs output beams will be superimposed with the five central orders of the DG (see Fig. 1). The optimized profile is fabricated in GaAs with UV optical lithography and ICP etching (see the SEM view in Fig. 2). The grating is then AR coated on both the etched and the rear facet. An experimental splitting efficiency of ∼75% (the theoretical value is 77%) is obtained along with a good uniformity between the five central orders intensities (see Fig. 2).

The CBC in N arms resonator is totally passive since it is only based on loss minimization in the external cavity. As explained in [9], the common cavity will ensure phase-locking between the different lasers and will select the proper longitudinal mode so that there are constructive interferences at the common output end (corresponding to the zeroth order of the DG) and destructive interferences on the other orders of the grating (some of them are represented by dashed lines in Fig. 1).

To maximize the combining efficiency of the DG, the intensities in the five arms should be equal. For that purpose, we need to know the current to be injected in each QCL, so they provide the same power to the five arm cavity. This question is not simple since the QCLs present different waveguide dimensions. Thus, the five QCLs are studied successively in an individual external cavity (IEC) with the same OC and the same length as in the five arm cavity. To simulate the 25% single pass losses caused by the DG, a 25/75 beamsplitter was introduced in the external arm of the IEC. For a particular value $P_{\text{single}}$ of the output power of the IEC, we deduce from the previous measurements a set of five currents quite different from the others because of the different waveguide dimensions used. Thus, for $P_{\text{single}} = 150 \text{ mW}$, the QCL currents are $I_i = [575, 510, 745, 760, 750] \text{ mA}$.

Then, the five arm cavity is characterized. For a particular value $P_{\text{single}}$, a set of currents $[I_i]$ is deduced and the output power $P_{\text{CBC}}$ in the combined beam is measured. Then, this process is repeated for different values of $P_{\text{single}}$. In Fig. 3, $P_{\text{CBC}}$ is represented according to $P_{\text{single}}$. The total power available from the five individual QCLs taking into account the DG losses, $P_{\text{available}} = 5$. $P_{\text{single}}$ is also represented. Moreover, we show on the same figure the power $P_{\text{potential}}$ that could have potentially been obtained from the five individual QCLs without the 25% additional losses. $P_{\text{potential}}$ is the sum of the output powers of the IEC without the 25/75 beamsplitter obtained for the same $I_i$.

An output power of 0.5 W was obtained in CW regime. The output power is quite stable (relative fluctuation < ±10% peak-to-peak at maximal power), at least over one hour of free running in nonprotected environment and no specific precaution (except QCL thermal stabilization). These power fluctuations were not observed when studying the CBC of two QCLs [6]. The increase of the output power fluctuations with the number of sources combined has already been described [10].

From Fig. 3, we deduce that ∼50% of the total available power, taking into account the DG losses, is effectively obtained in the combined beam ($P_{\text{CBC}}/P_{\text{available}} = 50\%$). Moreover, from the ratio $P_{\text{potential}}/P_{\text{available}}$, we deduce that the use of a 100% efficiency beam combiner would have increased $P_{\text{CBC}}$ by ∼65%. Thus, far more power could be obtained by using a multilevel phase grating or a continuous phase grating.

The loss of 50% of the available power is due to the fact the DG does not work at its maximal combining efficiency. The combining efficiency of the DG is defined as $\eta = I_0/\sum I_i$ with $I_i$ the intensity of the $i$th order between the DG and the OC (see Fig. 1). In Fig. 4, we show the calculated orders’ intensities of a DG illuminated by five beams with the proper relative phases along with the measured ones. A combining efficiency of ∼66% (see the inset in Fig. 3) is measured at maximal power. It means that 66% of the incoming energy on the DG from the five QCLs is effectively coupled into the zeroth order of the DG. As explained in [9], when the phase-locking between the five arms is perfect, the combining efficiency of the cavity should theoretically be equal to the splitting efficiency of the DG, which was measured to be $\eta_{\text{max}} = 75\%$.

We have determined two systematic errors that could explain the reduced CBC efficiency observed: the beam...
sizes error and the residual phase-mismatch between the arms. The differences between the beam sizes coming from the collimated QCLs are due to the different widths of the five QCLs waveguides. In [11], the CBC efficiency loss induced by beam profile nonuniformities is theoretically studied. In our case the combining efficiency is decreased to a value of $\eta \sim \eta_{\text{max}}$ 98% $\sim$ 73.5%. The other systematic error considered here is the residual phase-mismatches between the five arms. As explained before, passive CBC is only based on longitudinal mode selection in the $N$ arms resonator. If no common longitudinal mode (corresponding to a perfect synchronization between the $N$ arms) exists within the spectral gain bandwidth of the QCL, the system still selects the mode with the least losses. In this case, because of residual phase-mismatch between the $N$ arms, a part of the available power will be diffracted into the lossy orders of the DG, resulting in a reduced combining efficiency and thus a reduced output power [12]. If we assume a gain bandwidth of 100 cm$^{-1}$ and a typical arm length of $\sim$33 cm, we can estimate from [12] a combining efficiency of $\eta \sim \eta_{\text{max}}$ 93% $\sim$ 69.8%. If we add the contributions of the beam size differences and imperfect phase-locking, the combining efficiency should be reduced to $\eta \sim$68.5%. The value obtained with this approximate estimation of the CBC efficiency reduction is in good agreement with the measured combining efficiency of 66%. Thus the efficiency demonstrated appears to be close to the maximal value reachable given the experimental constraints. Errors such as beam positioning error, beam pointing error, or power nonuniformities are supposed to be controlled here.

Beam quality measurements on the output beam were performed with the scanning slit method on both the slow axis (the combining direction) and on the fast axis. The combined beam was still nearly diffraction-limited since the $M^2$ parameter (second-order moments definition) was measured to be $M^2_{\text{slow}} < 1.2$ and $M^2_{\text{fast}} < 1.6$. This $M^2$ value is very close to the one measured from the individual QCLs in external cavity ($M^2_{\text{slow}} < 1.2$ and $M^2_{\text{fast}} < 1.5$).

Finally, the spectral behavior of the cavity was analyzed using a spectrometer with a resolution of $\sim$1 nm (Fig. 5). The typical output spectrum presents narrow peaks spaced by $\sim$14 nm. Compared to a single QCL typical spectrum, we observe that only a few wavelengths could oscillate in the five arm resonator. Moreover, the peaks positions in wavelength along with their relative amplitudes are observed to be highly unstable. This is due to the fact that the system is continually compensating for the perturbations from the environment.

In this Letter, the coherent beam addition of five QCLs in an external cavity using a DG was demonstrated. A power of 0.5 W in continuous regime at RT and a combining efficiency of 66% were obtained while the combined beam exhibits the same beam quality as a single emitter ($M^2 < 1.6$). The method presented here is shown to be an efficient way to increase the brightness of QCLs and thus to address the power scaling issue in the midinfrared.

References